2/6

APPLICATION FOR FINANCIAL ASSISTANCE Revised 4/99

IMPORTANT: <u>Please consult the "Instructions for Completing the Project Application" for assistance in completion of this form.</u>

SUBDIVISION: City of Madeira		CODE# <u>061 - 4631</u> 2
DISTRICT NUMBER: 2 CO	OUNTY: Hamilton	DATE_11/26/08
CONTACT: Bruce G. Brandstetter	· · · · · · · · · · · · · · · · · · ·	513) 651-4224
(THE PROJECT CONTACT PERSON SHOULD BE THE INDIVIDUAL AND SELECTION PROCESS AND WHO CAN BEST ANSWER OR CO	. WIIO WILL BE AVAILABLE ON A DAY-TO-DAY BASISD IORDINATE THE RESPONSE TO QUESTIONS)	URING THE APPLICATION REVIEW
FAX_(513) 651-0147 E-	-MAIL_bbrandstetter@brands	tettercarroll.com
PROJECT NAME: KENWOOD ROAD F	RECONSTRUCTION, Euclid Road to	Kenwood Hills Drive
(Check only 1) (Check All Request	rand & Enter Amount) (Check Large rant \$1,125,000 x 1. ean 2. ean Assistance 3. 4. 5.	CT TYPE st Component) Road Bridge/Culvert Water Supply Wastewater Solid Waste Stormwater
TOTAL PROJECT COST: \$ 2,250,000.00		STED: \$1,125,000.00
DISTRIC To be completed	CT RECOMMENDATION d by the District Committee ONLY	
GRANT:\$ /, /25, 000 SCIP LOAN: \$ RA	LOAN ASSISTANCE:\$	
SCIP LOAN: \$ RA RLP LOAN: \$ RA	TE:% TERM TE:% TERM	yrs. yrs.
(Check only 1) X State Capital Improvement Program Local Transportation Improvements Program	Small Government Program	
FOR	OPWC USE ONLY	
PROJECT NUMBER: C /C	APPROVED FUNDING Loan Interest Rate: Loan Term: Maturity Date: Date Approved: SCIP Loan R	

1.0	PROJECT FINANCIAL INFORMATION		
1.1	PROJECT ESTIMATED COSTS: (Round to Nearest Dollar)	TOTAL DOLLARS	FORCE ACCOUNT DOLLARS
a.)	Basic Engineering Services:	\$	
	Preliminary Design \$		
	Final Design S		
	Bidding \$ Construction Phase \$		
	Additional Engineering Services	S	_
	*Identify services and costs below.		
b.)	Acquisition Expenses:		
	Land and/or Right-of-Way	S	
c.)	Construction Costs:	\$2,050,000.00	
d.)	Equipment Purchased Directly:	\$	•
e.)	Permits, Advertising, Legal:	S	_
	(Or Interest Costs for Loan Assistance Applications Only)		
f.)	Construction Contingencies:	\$ 200,000.00	-
g.)	TOTAL ESTIMATED COSTS:	\$	-
	Additional Engineering Services here:		
Servi	ee: Cost:		

	(Round to Nearest Dollar and Percent)		
		DOLLARS	%
a.)	Local In-Kind Contributions	\$	
b.)	Local Revenues	\$ 1,062,500.00	<u>47</u>
c.)	Other Public Revenues	\$	
	ODOT	\$	
	Rural Development	<u>\$</u>	
	OEPA	<u>\$</u>	
	OWDA	<u>\$</u>	
	CDBG OTHER <u>MRF</u>	\$ \$ 62,500.00	
	OTHER WIRE	<u>5 02,500.00</u>	3_
	SUBTOTAL LOCAL RESOURCES:	\$ 1,125,000.00	50
d.)	OPWC Funds		
,	1. Grant	\$ 1,125,000.00	50
	2. Loan	\$	
	3. Loan Assistance	\$	
	SUBTOTAL OPWC RESOURCES:	\$ 1,125,000.00	50
e.)	TOTAL FINANCIAL RESOURCES:	\$ 2,250,000.00	100%
1.3	AVAILABILITY OF LOCAL FUNDS	:	
	Attach a statement signed by the <u>Chiel</u> funds required for the project will be a Schedule section.		
	ODOT PID# Sale	Datas	
	STATUS: (Check one)	Date.	
	Traditional		
	Local Planning Agend	cy (LPA)	
	State Infrastructure I	Bank	
	Treeth velve make tracke to		

PROJECT FINANCIAL RESOURCES:

1.2

	project is multi-jurisdictional, information must be <u>consolidated</u> in this section.
PR	ROJECT NAME: KENWOOD ROAD RECONSTRUCTION
BR	RIEF PROJECT DESCRIPTION - (Sections a through d):
A:	SPECIFIC LOCATION:
	This project is located on Kenwood Road, from Euclid Road to the south corporation lin Kenwood Hills Drive. Complete roadway reconstruction is planned for the entire length the project except the section from Whetsel Avenue to the south corporation limits.
B:	PROJECT ZIP CODE: 45243 PROJECT COMPONENTS:
	The complete reconstruction of Kenwood Road from Euclid Road to Whetsel Avenuation This includes removal of existing pavement and curbing and replacing it with neconcrete curb and a full-depth asphalt pavement. The storm sewer system will upgraded. The section from Whetsel Avenue to the south corporation line will receipt drainage improvements and pavement rehabilitation.
	A waterline replacement project, 8200 LF, is currently under construction. The alignme of the waterline is generally down the centerline of the road. This will result in trench cualong the entire length of the project which will lead to future pavement failures.
C:	PHYSICAL DIMENSIONS / CHARACTERISTICS:
	The existing pavement is in critical condition. New water and sewer lines are planned for construction over the next 8 months. This project will complement the utility projects. Concrete curbs are deteriorating and there are many areas of pavement failures. The overall dimensions are 4300' x 37'.
	Concrete Sidewalk 22,000 LF Concrete curbs 8,500 LF Full-Depth Pavement 17,300 SY Storm Pipe Replacement 300 LF Inlet Replacement 12 EA
D:	DESIGN SERVICE CAPACITY:
Deta	nil current service capacity versus proposed service level.
	This is a reconstruction project and will not affect capacity.
Roac	d or Bridge: Current ADT 11.291 Year: 2007 Projected ADT: 17.455 Year: 2029

2.3 USEFUL LIFE/COST ESTIMATE: Project Useful Life: 20 Years.

Stormwater: Number of households served:_____

Attach <u>Registered Professional Engineer's</u> statement, with <u>original seal and signature</u> confirming the project's useful life indicated above and estimated cost.

3.0 REPAIR/REPLACEMENT or NEW/EXPANSION:

TOTAL PORTION OF PROJECT REPAIR/REPLACEMENT \$2,105,000 93.5 %

TOTAL PORTION OF PROJECT NEW/EXPANSION \$ 146,250 6.5 % (concrete sidewalk)

4.0 PROJECT SCHEDULE: *

		BEGIN DATE	END DATE
4.1	Engineering/Design:	01 / 01 / 09	05 / 01 / 09
4.2	Bid Advertisement and Award:	05 / 01 / 09	07 / 01 / 09
4.3	Construction:	07 / 01 / 09	12 / 31 / 10
4.4	Right-of-Way/Land Acquisition	N/A	N/A

^{*} Failure to meet project schedule may result in termination of agreement for approved projects. Modification of dates must be requested in writing by the CEO of record and approved by the commission once the Project Agreement has been executed. The project schedule should be planned around receiving a Project Agreement on or about July 1st.

5.0 APPLICANT INFORMATION:

5.1	CHIEF EXECUTIVE OFFICER TITLE STREET	Thomas W. Moeller City Manager 7141 Miami Avenue
	CITY/ZIP	Madeira, Ohio 45243
	PHONE FAX	513/561-7228 513/272-4211
5.2	CHIEF FINANCIAL OFFICER TITLE STREET	Steve Soper Treasurer 7141 Miami Avenue
	CITY/ZIP PHONE FAX	Madeira, Ohio 45243 513/561-7228 513/272-4211
5.3	PROJECT MANAGER TITLE STREET	Bruce G. Brandstetter, P.E. Brandstetter Carroll Inc. 424 East Fourth Street
	CITY/ZIP PHONE FAX	Cincinnati, Ohio 45202 513/651-4224 513/651-0147

Changes in Project Officials must be submitted in writing from the CEO.

6.0 ATTACHMENTS/COMPLETENESS REVIEW:

Check each section below, confirming that each item listed is attached.

- X. A certified copy of the legislation by the governing body of the applicant authorizing a designated official to sign and submit this application and execute contracts. This individual should sign under 7.0, Applicant Certification, below.
- A certification signed by the applicant's chief financial officer stating all local share funds required for the project will be available on or before the dates listed in the Project Schedule section. If the application involves a request for loan (RLP or SCIP), a certification signed by the CFO which identifies a specific revenue source for repaying the loan also must be attached. Both certifications can be accomplished in the same letter.
- A registered professional engineer's detailed cost estimate and useful life statement, as required in 164-1-13, 164-1-14 and 164-1-16 of the Ohio Administrative Code. Estimates shall contain engineer's <u>original seal or stamp and signature</u>.
- N/A A cooperation agreement (if the project involves more than one subdivision or district) which identifies the fiscal and administrative responsibilities of each participant.
- N/A Projects which include new and expansion components and potentially affect productive farmland should include a statement evaluating the potential impact. If there is a potential impact, the Governor's Executive Order 98-VII and the OPWC Farmland Preservation Review Advisory apply.
- _x Capital Improvements Report: (Required by 164 O.R.C. on standard form)
- _x_ Supporting Documentation: Materials such as additional project description, photographs, economic impact (temporary and/or full time jobs likely to be created as a result of the project), accident reports, impact on school zones, and other information to assist your district committee in ranking your project. Be sure to include supplements which may be required by your *local* District Public Works Integrating Committee.

7.0 APPLICANT CERTIFICATION:

The undersigned certifies that: (1) he/she is legally authorized to request and accept financial assistance from the Ohio Public Works Commission; (2) that to the best of his/her knowledge and belief, all representations that are part of this application are true and correct; (3) that all official documents and commitments of the applicant that are part of this application have been duly authorized by the governing body of the applicant; and, (4) should the requested financial assistance be provided, that in the execution of this project, the applicant will comply with all assurances required by Ohio Law, including those involving Buy Ohio, and prevailing wages.

IMPORTANT: Applicant certifies that physical construction on the project as defined in the application has NOT begun, and will not begin until a Project Agreement on this project has been executed with the Ohio Public Works Commission. Action to the contrary will result in termination of the agreement and withdrawal of Ohio Public Works Commission funding of the project.

Thomas W. Moeller, City Manager	
Certifying Representative (Type or Prin	t Name and Title)
Thomas W. Malle	9-17-08
Signature/Date Signed	

CITY OF MADEIRA

Thomas W. Moeller City Manager 7141 Miami Avenue • Cincinnati, Ohio 45243-2699 (513) 561-7228 • Fax (513) 272-4211

December 1, 2008

District Two Integrating Committee Hamilton County Engineer's Office 138 East Court Street Cincinnati, OH 45202

Attention: Joe Cottrill

RE: City of Madeira

SCIP Application/FY09 (Revised)

Kenwood Road Improvement Project

Ladies/Gentlemen:

It is hereby certified that the local matching funds in the amount of \$1,062,500 for the above referenced project will be appropriated in the FY09 Budget. It is understood we will receive an amount of \$62,500 in Municipal Road Funds for this project. We also understand this project will be funded in 2009 and the City will be prepared to meet the scheduling deadlines stated within the approved application. We will be expected to submit another application for the 2010 funding round to complete the project.

Thank you for your time and consideration. Please call me if you have any questions.

Sincerely,

Monas W. Maeller

City Manager

c: Bruce Brandstetter, City Engineer

SCIP FY09 Kenwood Road Project 08dec01

rikasi kecelariyi.

han ikinga janging merapadakan salapatolog

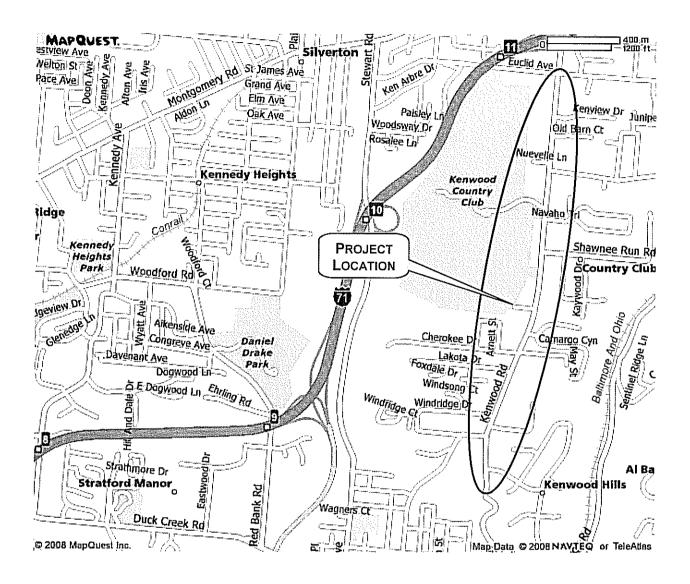
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PRELIMINARY OPINION OF PROBABLE COST KENWOOD ROAD MADEIRA, OHIO Revised November 25, 2008 08006

							00000
DEGODINE					UNIT		
DESCRIPTION	QUANTITY	UNIT		(COST		TOTAL
Pavement Removal	47.454		_	_			
Roadway	17,150	SY	@		0.00	\$	171,500.00
Driveway	200	SY	@		0.00		2,000.00
Excavation	2,700	CY	@	3	0.00		81,000.00
New Full Depth Pavement-Euclid to Whetsel							
8" Bituminous Aggregate Base	4,000	CY	@	13	0.00		520,000.00
2-1/2" Asphalt Concrete, Leveling	1,250	CY	@	14	5.00		181,250.00
1-1/2" Asphalt Concrete, Surface	750	CY	@	15	0.00		112,500.00
Concrete Curb	8,500	LF	@	2	5.00		212,500.00
Driveways	1,800	SY	@	4	0.00		72,000.00
6" Gravel Base (Drainage Layer)	3,150	CY	@	4	0.00		126,000.00
Geotextile Fabric	17,150	SY	@		2.50		42,875.00
Asphalt Leveling and Surface Course	100	CY	@	15	0.00		15,000.00
(Whetsel to Kenwood Hills Dr.)							
Concrete Sidewalk	22,000	SF	@		5.00		110,000.00
Modular Wall at Sidewalk	1,100	SF	@	2	2.00		24,200.00
Manhole Adjustments	1	LS	@	3,67	5.00		3,675.00
Underdrains	8,500	LF	@	1	5.00		127,500.00
Storm Inlet Reconstruction / Replacement	12	EA	@	1,50	0.00		18,000.00
Storm Pipe Replacement	300	LF	@	•	0.00		30,000.00
Subgrade Excavation/Replacement	2,150	CY	@		0.00		107,500.00
Downspout Pipe	100	LF	@		5.00		1,500.00
Pavement Markings	1	LS	@	25,00			25,000.00
Seed and Mulch	2,000	SY	@		2.00		4,000.00
Topsoil	250	CY	@		0.00		10,000.00
Mobilization	1	LS	@	12,50			12,500.00
Construction Staking	1	LS	@	14,50			14,500.00
Maintenance of Traffic	1	LS	@	25,00			25,000.00
Sub-Total			•		•	\$	2,050,000.00
Contingency						\$	200,000.00
Total					=		
Total					182021	M	مراراً المالية
This is to certify that this project, upon satisfac		ion and					0F 0H/

normal environmental and climatic conditions will have a useful life of 20 years:

PROJECT LOCATION



PY 2009 SCIP APPLICATION September 19, 2008

KENWOOD ROAD
Euclid Road to Kenwood Hills Drive
MADEIRA, OHIO

ORDINANCE NO. 08-38

AUTHORIZING THE CITY MANAGER TO SUBMIT AN APPLICATION FOR STATE CAPITAL IMPROVEMENT PROGRAM (SCIP) FUNDS FOR THE KENWOOD ROAD RESURFACING IMPROVEMENTS PROJECT

WHEREAS, it is determined that Kenwood Road is in need of resurfacing improvements; and

WHEREAS, the State Capital Improvement Program will fund work on the aforementioned street; and

WHEREAS, the City Manager recommends that we submit an application for this project.

NOW, THEREFORE, BE IT ORDAINED by the Council of the City of Madeira, State of Ohio:

<u>Section 1.</u> That the City Manager is hereby authorized to submit an application to the State Capital Improvement Program District Integrating Committee for funding under the State Capital Improvement Program for the Kenwood Road Resurfacing Improvements Project.

Section 2. That this Ordinance shall take effect from and after the earliest period allowed by law.

PASSED ON THE 8TH DAY OF SEPTEMBER, 2008 BY THE FOLLOWING 5-0 VOTE:

YEA: NAY: ABSTAIN: ABSENT:
Ken Born
Tim Dicke
Sarah Evans
Dave Sams

NAY: ABSTAIN: ABSENT:
Rick Brasington
John Dobbs

Sarah A. Evans, Mayor

Rick Staubach

Diane D. Novakov, Clerk of Council

CERTIFICATE OF COPY

STATE O	F OHIO				
	Madeira Hamilton	<u>SS</u>			
that the for Authority of of such ord a referendu publication	egoing is a true and the said City on in inance be made and upon such ordinates of rec	d correct copy of the <u>8th</u> day o id certified of rec nance have been ord in Ordinance EOF, I have here	Ordinance No. f September ord according to taken; and that s No. 08-38,Page	oira,Ohio do here 08-38 adopted by the legi,	slative ublications s looking to icate of
			<u>Man</u> Diane D.	C. M. Morako Novakov, Clerk of Counci	<u>/</u>
			City of	Madeira	. Ohio

HAMILTON COUNTY ENGINEER'S OFFICE

PROJECT APPLICATION - MUNICIPAL ROAD FUND - 2009

IN	STR	UCTIONS:	Municipality	ality 's ch	each project. 's Engineer, or oosing shall pr by 4:00 p.m.,	a registered E	ngine icatio	er of the	
1.	Mu	nicipality			ity of Madeir	a, Ohio	_		
2.	Roa	ad Name	Ken	Noo	d Road				
3.	Pro	ject Limits	Eucl (Please give a	id to 1 "fro	South Corpo om – to" limit	ration Line (P if possible.)	<u>Сепу</u>	ood Hills Dr	ive)
4.	Pro	ject Priority	One						
5.	Pre	sent Roadway D	ata: (Answer	alI ti	nat apply)				
	a.	Pav't Width	37	b.	R/W Width	60'	c.	Curb Type	Integral with
	d.	Type Surface	Asphalt	e,	Type Base	Concrete	f.	Shldr Type	Pavement N/A
	g.	Shldr Width	N/A	h.	Year Last Res	surfaced	19	93	
6.	Pre	sent condition o	f project area:	List	deficiencies &	reasons for im	prov	ement.	
	wid rep	ened by 8 feet	, 6 inches on	eac	h eide in 104	are primarily	alon	g the longit	rs) in 1993. It deteriorated udinal joints where it was ed concrete. A waterline cts will add to the already
7.	Proj part	ject description iculars. <u>List als</u> e	or statement o	f wo	rk to be done: n" technology/	Include width	and ruetic	type of new on methods th	pavement and other project at will be used in this project.
	Nev ten	v pavement sha inches of cond	all be the same rete. Storm s	e wie struc	dth. Total rec tures and sto	onstruction is rm pipe shall	proj be r	posed with s eplaced and	six-inch granular base and under drains provided.
	Wai	rm asphalt sha	ll be used for	the:	surface cours	e.			
8.	Trai	ffic Data <u>:</u>	a. Present	Vol	ume <u>11,3</u>	<u>00</u> b. D	ate o	f Count	8/07
9.	Cos	t Estimate <u>:</u>			•				
	Who	en engineering p	olans are neces	sary,	list the follow	ing costs:			
		a. Prepara	tion of prelimi	пагу	plans and esti	mate, etc.			\$ 110,000
		b. Prepara	tion of final pl	ans d	& estimate, etc				\$ <u>160.000</u>
		c. Constru	ction Cost Est	imat	e				\$ 4.500,000
		d. Other C	Costs (Specify)		Construction A	Administration			\$ 135,000
		TOTAL AMO	UNT OF MRI	FL	<u>NDS</u> APPLII	ED FOR			\$125,000
10.	Esti	mated date cons	truction can be	star	ted after appro	val <u>Ju</u>	ly, 2	009	
11.	Estir	mated date cons	truction can be	star	ted <u>if not</u> fund	ed 100% from	MRF		
12.	Are	the MRF funds	to be used as n	natel	ing funds for	SCIP/LTIP?	_>	not avail	able No
	If ye	s, what percents	ige of the proje	ect co	ost? <u>3</u>	%			
13.	Cost	Estimate Prepa	red by: Bruce	e Bra	indstelled	D	ate:_	August 29, 2	2008
14.	Арр	lication Prepare	d by:			D	ate: _	B/29	<u> 108</u>

Make copies of this form as needed. 2009 MRF Form

SUMMARY SHEET KENWOOD ROAD TRAFFIC COUNTS MADEIRA, OHIO September 12, 2008 08006

BRANDSTETTER CARROLL INC. Architects Engineers Planners

Kenwood Road, near Euclid

Southbound 5,542 24-hour count
Northbound 5,749 24-hour count
11,291 Bi-Directional ADT

The following data was collected on August 29 and 30, 2007. This information is certified to be accurate.

Note: Updated counts were not taken in 2008 due to the various, adjacent projects (Whetsel Avenue Sanitary Sewer, Shawnee Run Road Reconstruction, Kenwood Road Waterline and Kenwood Road (City of Cincinnati) Water and Sewer Extensions. Traffic counts taken in 2008 would not be accurate as a result of these projects.

BEB:djb

Kenwood Road near Euclid Start Date: 8/29/2007 Start Time: 12:30:00 PM

	NB Kenwood Road	SB Kenwood Road	Total Volume
8/29/2007 12:30 PM	72	90	162
8/29/2007 12:45 PM	120	70	190
8/29/2007 01:00 PM	69	69	138
8/29/2007 01:15 PM	100	86	186
8/29/2007 01:30 PM	90	87	177
8/29/2007 01:45 PM	100	108	208
8/29/2007 02:00 PM	94	86	180
8/29/2007 02:15 PM	98	104	202
8/29/2007 02:30 PM	100	121	221
8/29/2007 02:45 PM	109	115	224
8/29/2007 03:00 PM	108	131	239
8/29/2007 03:15 PM	86	132	218
8/29/2007 03:30 PM	84	120	204
8/29/2007 03:45 PM	102	136	238
8/29/2007 04:00 PM	81	127	208
8/29/2007 04:15 PM	105	141	246
8/29/2007 04:30 PM	112	142	254
8/29/2007 04:45 PM	130	122	252
8/29/2007 05:00 PM	112	132	244
8/29/2007 05:15 PM	120	130	250
8/29/2007 05:30 PM	76	122	198
8/29/2007 05:45 PM	81	74	155
8/29/2007 06:00 PM	69	87	156
8/29/2007 06:15 PM	82	79	161
8/29/2007 06:30 PM	66	82	148
8/29/2007 06:45 PM	60	70	130
8/29/2007 07:00 PM	56	83	139
8/29/2007 07:15 PM	45	55	100
8/29/2007 07:30 PM	50	58	108
8/29/2007 07:45 PM	52	69	121
8/29/2007 08:00 PM	37	73	110
8/29/2007 08:15 PM	32	60	92
8/29/2007 08:30 PM	41	55	96
8/29/2007 08:45 PM	30	28	58 ·
8/29/2007 09:00 PM	27	38	65
8/29/2007 09:15 PM	18	42	60
8/29/2007 09:30 PM	16	20	36
8/29/2007 09:45 PM	13	19	32
8/29/2007 10:00 PM	12	20	32
8/29/2007 10:15 PM	14	11	25
8/29/2007 10:30 PM	4	14	18
8/29/2007 10:45 PM	6	7	13
8/29/2007 11:00 PM	6	13	19
8/29/2007 11:15 PM	10	6	16
8/29/2007 11:30 PM	6	6	12
8/29/2007 11:45 PM	1	8	9
8/30/2007 12:00 AM	0	3	3
8/30/2007 12:15 AM	3	5	8
8/30/2007 12:30 AM	3	5	8

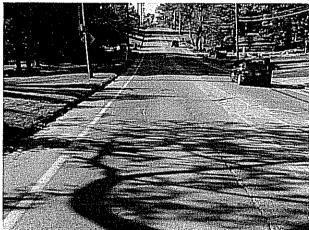
Kenwood Road near Euclid Start Date: 8/29/2007 Start Time: 12:30:00 PM

8/30/2007 12:45 AM	1	5	6
8/30/2007 01:00 AM	1	4	5
8/30/2007 01:15 AM	1	0	1
8/30/2007 01:30 AM	1	2	3
8/30/2007 01:45 AM	3	3	6
8/30/2007 02:00 AM	1	4	5
8/30/2007 02:15 AM	3	0	3
8/30/2007 02:30 AM	0	1	1
8/30/2007 02:45 AM	2	1	3
8/30/2007 03:00 AM	2	2	4
8/30/2007 03:15 AM	4	1	5
8/30/2007 03:30 AM	7	1	8
8/30/2007 03:45 AM	4	2	6
8/30/2007 04:00 AM	5	3	8
8/30/2007 04:15 AM	8	2	10
8/30/2007 04:30 AM	12	7	19
8/30/2007 04:45 AM	22	15	37
8/30/2007 05:00 AM	20	7	27
8/30/2007 05:15 AM	45	21	66
8/30/2007 05:30 AM	58	26	84
8/30/2007 05:45 AM	82	43	125
8/30/2007 06:00 AM	94	52	146
8/30/2007 06:15 AM	124	47	171
8/30/2007 06:30 AM	135	59	194
8/30/2007 06:45 AM	138	84	222
8/30/2007 07:00 AM	126	69	195
8/30/2007 07:15 AM	132	67	199
8/30/2007 07:30 AM	124	75	199
8/30/2007 07:45 AM	130	68	198
8/30/2007 08:00 AM	90	68	158
8/30/2007 08:15 AM	72	47	119
8/30/2007 08:30 AM	82	58	140
8/30/2007 08:45 AM	87	64	151
8/30/2007 09:00 AM	7 6	68	144
8/30/2007 09:15 AM	78	70	148
8/30/2007 09:30 AM	61	63	124
8/30/2007 09:45 AM	85	77	162
8/30/2007 10:00 AM	92	72	164
8/30/2007 10:15 AM	108	91	199
8/30/2007 10:30 AM	88	70	158
8/30/2007 10:45 AM	95	79	174
8/30/2007 11:00 AM	76	116	192
8/30/2007 11:15 AM	92	104	196
8/30/2007 11:30 AM	78	68	146
8/30/2007 11:45 AM	96	74	170
8/30/2007 12:00 PM	81	96	177
8/30/2007 12:15 PM	80	88	168
8/30/2007 12:30 PM	39	37	76
24 Hour Total	5749	5542	11291
21,100, 100	OT TO	JUTE	11231













ADDITIONAL SUPPORT INFORMATION

For Program Year 2009 (July 1, 2009 through June 30, 2010), applying agencies shall provide the following support information to help determine which projects will be funded. Information on this form must be accurate, and where called for, based on sound engineering principles. Documentation to substantiate the individual items, as noted, is required. The applicant should also use the rating system and its' addendum as a guide. The examples listed in this addendum are not a complete list, but only a small sampling of situations that may be relevant to a given project.

IF YOU ARE APPLYING FOR A GRANT, WILL YOU BE WILLING TO ACCEPT A LOAN IF ASKED BY THE DISTRICT? YES X NO (ANSWER REQUIRED)

Note: Answering "Yes" will not increase your score and answering "NO" will not decrease your score.

1) What is the physical condition of the existing infrastructure that is to be replaced or repaired?

Give a statement of the nature of the deficient conditions of the present facility exclusive of capacity, serviceability, health and/or safety issues. If known, give the approximate age of the infrastructure to be replaced, repaired, or expanded. Use documentation (if possible) to support your statement. Documentation may include (but is not limited to): ODOT BR86 reports, pavement management condition reports, televised underground system reports, age inventory reports, maintenance records, etc., and will only be considered if included in the original application.

The existing pavement is in critical condition, it was constructed in 1949. Utility cuts, along with the overall deterioration of the pavement and concrete curbs, have resulted in a pavement that is in critical condition. The existing pavement was widened in 1949 and is 8" thick concrete with a 2" asphalt overlay. Per the enclosed Geotechnical Report by the H.C. Nutting Company dated September 2007, the subgrade has deteriorated and is the major cause of failure. The subgrade can only be corrected by full-depth reconstruction. Please see pages 11,12, 13 and 14. Now with the waterline replacement project (8200 LF), the condition of the pavement will deteriorate more quickly.

2) How important is the project to the safety of the Public and the citizens of the District and/or service area?

Give a statement of the projects effect on the safety of the service area. The design of the project is intended to reduce existing accident rate, promote safer conditions, and reduce the danger of risk, liability or injury. (Typical examples may include the effects of the completed project on accident rates, emergency response time, fire protection, and highway capacity.) Please be specific and provide documentation if necessary to substantiate the data. The applicant must demonstrate the type of problems that exist, the frequency and severity of the problems and the method of correction.

This roadway is a primary north-south connector between Madeira, Columbia and Sycamore Townships. The proposed construction will include storm pipe and inlet replacement. Due to the pavement failures, the roadway is becoming unsafe to the traveling public. The current water and sewer projects will add to the pavement deterioration.

3) How important is the project to the health of the Public and the citizens of the District and/or service area?

Give a statement of the projects effect on the health of the service area. The design of the project will improve the overall condition of the facility so as to reduce or eliminate potential for disease, or correct concerns regarding the environmental health of the area. (Typical examples may include the effects of the completed project by improving or adding storm drainage or sanitary facilities, etc.). Please be specific and provide documentation if necessary to substantiate the data. The applying agency must demonstrate the type of problems that exist, the frequency and severity of the problems and the method of correction.

N/A	

MRF funds have been applied for \$ 125,000.00
The information regarding local matching funds is to be filed by the applying agency in Section 1.2 (c) of the Ohio Public Works Association's "Application For Financial Assistance" form. If MRF funds are being used for matching funds, the MRF application must have been filed by Friday , August 29 , 2008 for this project with the Hamilton County Engineer's Office. List below all "other" funding the source(s).
8) Matching Funds - OTHER
The information regarding local matching funds is to be filed by the applicant in Section 1.2 (b) of the Ohio Public Works Association's "Application For Financial Assistance" form.
7) Matching Funds - LOCAL
the residential area of Madeira to the commercial redevelopment in Sycamore Township.
that is taking place all along Kenwood Road, from the highrise construction in the City of Cincinnati thru
the right-of-way in good condition so as to preserve property values and encourage the redevelopment
Give a statement of the projects effect on economic growth (be specific). It is important to keep the payement and drainage in good condition. The City needs to maintain
6) Economic Growth – How will the completed project enhance economic growth
· · · · · · · · · · · · · · · · · · ·
(example: rates for water or sewer, frontage assessments, etc.).
5) To what extent will the user fee funded agency be participating in the funding of the project?
Priority 5
Priority 4
Priority 3
Priority 2
Priority 1Kenwood Road Reconstruction
The applying agency must_submit a listing in priority order of the projects for which it is applying. Points will be awarded on the basis of most to least importance.

4) Does the project help meet the infrastructure repair and replacement needs of the applying jurisdiction?

Describe how the proposed project will alleviate serious capa Project will eliminate pavement failures, rep		•	•	•	oles an	ıd_storm_in	lets,
and eliminate ponding of water. These improvement	ts will m	naintain_	r,boog	ıninterru	oted ve	hicular, bicy	/cle,
and pedestrian traffic.							
Level of Service (LOS) calculations shall be for the improven of a larger project then any preceding phases shall be conside project phases shall not be considered as part of this applicati	red existi	ing condit	ions for				ise
For roadway betterment projects, provide the existing and promethodology outlined within AASHTO'S "Geometric Design Highway Capacity Manual.							
No Build		Prop	osed G	eometry.			
Current Year LOS		Currer	it Year I	Los			
Design Year LOS		Desig	n Year I	LOS			
10) If SCIP/LTIP funds are granted, when would the const. If SCIP/LTIP funds are awarded, how soon after receiving the year following the deadline for applications) would the project of previous projects to help judge the accuracy of a jurisdiction. Number of months	Project A be under	greement contract?	from O	PWC (tent ipport Staf			
a.) Are preliminary plans or engineering completed?	Yes	x	_ No		N/A		
b.) Are detailed construction plans completed?	Yes		_ No	x	N/A		
c.) Are all utility coordination's completed?	Yes		_ No	_X	N/A		
d.) Are all right-of-way and easements acquired (if applicable)?	Yes		_ No		N/A	<u>X</u>	
If no, how many parcels needed for project?	Of thes	e, how ma	ıny are:	Takes			
			Tem	рогагу		-	
			Perm	anent		_	
For any parcels not yet acquired, explain the status of the	he ROW	acquisitio	n proces	s for this p	roject.		
			<u> </u>				
e.) Give an estimate of time needed to complete any item above	not yet co	ompleted.			4	_ months.	

9) Will the project alleviate serious capacity problems or hazards or respond to the future level of service needs of the

district?

11) Does the infrastructure have regional impact?			
Give a brief statement concerning the regional significance of the infrastructure to be replaced, repaired, or expanded. The overall project has regional impact in so far as it serves not only the City of Madeira, but also			
the City of Cincinnati, Columbia Township and Sycamore Township. It also is a major north-south			
connector for i-71.			
12) What is the overall economic health of the jurisdiction?			
The District 2 Integrating Committee predetermines the jurisdiction's economic health. The economic health of a jurisdiction may periodically be adjusted when census and other budgetary data are updated.			
13) Has any formal action by a federal, state, or local government agency resulted in a partial or complete ban of the usage or expansion of the usage for the involved infrastructure?			
Describe what formal action has been taken which resulted in a ban of the use of or expansion of use for the involved infrastructure? Typical examples include weight limits, truck restrictions, and moratoriums or limitations on issuance of building permits, etc. The ban must have been caused by a structural or operational problem to be considered valid. Submission of a copy of the approved legislation would be helpful. No Ban			
Will the ban be removed after the project is completed? YesNoN/Ax			
14) What is the total number of existing daily users that will benefit as a result of the proposed project?			
For roads and bridges, multiply current Average Daily Traffic (ADT) by 1.20. For inclusion of public transit, submit documentation substantiating the count. Where the facility currently has any restrictions or is partially closed, use documented traffic counts prior to the restriction. For storm sewers, sanitary sewers, water lines, and other related facilities, multiply the number of households in the service area by 4. User information must be documented and certified by a professional engineer			

uit ď ıe er or the jurisdictions' C.E.O.

Traffic: ADT <u>11,291</u> X 1.20 = <u>13,549</u> Users Homes _____ X 4.00 = ____ Users Water/Sewer:

15) Has the jurisdiction enacted the optional \$5 license plate fee, an infrastructure levy, a user fee, or dedicated tax for the pertinent infrastructure?

The applying jurisdiction shall list what type of fees, levies or taxes they have dedicated toward the type of infrastructure being applied for.

Optional \$5.00 License Ta	ax <u> </u>	
Infrastructure Levy	-	Specify type
Facility Users Fee		Specify type
Dedicated Tax		Specify type
Other Fee, Levy or Tax	· · · · · · · · · · · · · · · · · · ·	Specify type

SCIP/LTIP PROGRAM **ROUND 23 - PROGRAM YEAR 2009** PROJECT SELECTION CRITERIA **JULY 1, 2009 TO JUNE 30, 2010**

NAME OF APPLICANT: MADEIZA	
NAME OF PROJECT: KENWOOD RD RECONST	
RATING TEAM: 5	

General Statement for Rating Criteria

Points awarded for all items will be based on engineering experience, field verification, application information and other information supplied by the applying agency, which is deemed to be relevant by the Support Staff. The examples listed in this addendum are not a complete list, but only a small sampling of situations that may be relevant to a given project.

CIRCLE THE APPROPRIATE RATING

What is the physical condition of the existing infrastructure that is to be replaced or repaired?

25 - Failed **Appeal Score**

23, - Critical 20 Very Poor 17 - Poor

1)

15 - Moderately Poor

10 - Moderately Fair

5 - Fair Condition

0 - Good or Better

Criterion 1 - Condition

Condition of the particular infrastructure to be repaired, reconstructed or replaced shall be a measure of the degree of reduction in condition from its original state. Historic pavement management data based on ASTM D6433-99 rating system may be submitted as documentation. Capacity, serviceability, safety and health shall not be considered in this criterion. Any documentation the Applicant wishes to be considered must be included in the application package.

Definitions:

Failed Condition - requires complete reconstruction where no part of the existing facility is salvageable. (E.g. Roads: complete reconstruction of roadway, curbs and base; Bridges: complete removal and replacement of bridge; Underground: removal and replacement of an underground drainage or water system.

Critical Condition - requires partial reconstruction to maintain integrity. (E.g. Roads: reconstruction of roadway/curbs can be saved; Bridges: removal and replacement of bridge with abutment modification; Underground: removal and replacement of part of an underground drainage or water system.

Very Poor Condition - requires extensive rehabilitation to maintain integrity. (E.g. Roads: extensive full depth, partial depth and curb repair of a roadway with a structural overlay; Bridges: superstructure replacement; Underground: repair of joints and/or replacement of pipe sections.

Poor Condition - requires standard rehabilitation to maintain integrity. (E.g. Roads: moderate full depth, partial depth and curb repair to a roadway with no structural overlay needed or structural overlay with minor repairs to a roadway needed; Bridges: extensive patching of substructure and replacement of deck; Underground: insituform or other in ground repairs.

Moderately Poor Condition - requires minor rehabilitation to maintain integrity. (E.g. Roads: minor full depth, partial depth or curb repairs to a roadway with either a thin overlay or no overlay needed; Bridges: major structural patching and/or major deck repair.

Moderately Fair Condition - requires extensive maintenance to maintain integrity. (E.g. Roads: thin or no overlay with extensive crack sealing, minor partial depth and/or slurry or rejuvenation; Bridges: minor structural patching, deck repair, erosion control.)

Fair Condition - requires routine maintenance to maintain integrity. (E.g. Roads: slurry seal, rejuvenation or routine crack sealing to the roadway; Bridges: minor structural patching.)

Good or Better Condition - little to no maintenance required to maintain integrity.

Note: If the infrastructure is in "good" or better condition, it will NOT be considered for SCIP/LTIP funding unless it is an expansion project that will improve serviceability.

How important is the project to the safety of the Public and the citizens of the District and/or ser	vice area?
25 - Highly significant importance 20 - Considerably significant importance 15 - Moderate importance 10 - Minimal importance 5 - Poorly documented importance 0 - No measurable impact	Appeal Score
Criterion 2 – Safety The applying agency shall include in its application the type of deficiency that currently exists and improve the situation. For example, have there been vehicular accidents attributable to the proble injuries or fatalities? In the case of water systems, are existing hydrants non-functional? In the ca capacity inadequate to provide volumes or pressure for adequate fire protection? In all cases, speci. Mentioned problems, which are poorly documented, generally will not receive more than 5 points.	ems cited? Have they involved se of water lines, is the present
Note: Each project is looked at on an individual basis to determine if any aspects of this category ap NOT intended to be exclusive.	ply. Examples given above are
How important is the project to the <u>health</u> of the Public and the citizens of the District and/or ser	vice area?
25 - Highly significant importance 20 - Considerably significant importance 15 - Moderate importance 10 - Minimal importance 5 - Poorly documented importance No measurable impact	Appeal Score
Criterion 3 – Health The applying agency shall include in its application the type, frequency, and severity of the health probreduced by the intended project. For example, can the problem be eliminated only by the project, or satisfactory? If basement flooding has occurred, was it storm water or sanitary flow? What complain case of underground improvements, how will they improve health if they are storm sewers? How with improve health or reduce health risk? In all cases, quantified documentation is required. Mention documented, generally will not receive more than 5 points.	would routine maintenance be nts if any are recorded? In the rould improved sanitary sewers
Note: Each project is looked at on an individual basis to determine if any aspects of this category appare NOT intended to be exclusive.	oly. Examples given above
Does the project help meet the infrastructure repair and replacement needs of the applying agenc Note: Applying agency's priority listing (part of the Additional Support Information) must be filed with appl	y? lication(s).
25 First priority project 20 - Second priority project 15 -Third priority project 10 - Fourth priority project 5 - Fifth priority project or lower	Appeal Score
Criterion 4 – Jurisdiction's Priority Listing	

2)

3)

The applying agency must submit a listing in priority order of the projects for which it is applying. Points will be awarded on the basis of most to least importance. The form is included in the Additional Support Information.

)	<u>To</u> what extent will a user fee funded agency be	participating in the funding of the project?
-	(10) Less than 10%	
	9-10% to 19.99%	
	8 – 20% to 29.99%	Appeal Score
	7 – 30% to 39.99%	**
	6 – 40% to 49.99%	
	5 – 50% to 59.99%	
	4 – 60% to 69.99%	
	3 – 70% to 79.99%	
	2 – 80% to 89.99%	
	1 – 90% to 95%	
	0 – Above 95%	•

Criterion 5 - User Fee-funded Agency Participation

To what extent will a user fee funded agency be participating in the funding of the project? (Example: rates for water or sewer, frontage assessments, etc.). The applying agency must submit documentation.

6) Economic Growth – How the completed project will enhance economic growth (See definitions).

10 - The project will directly secure new employment	Appeal Score
— The project will permit more development	
0 The project will not impact development	

Criterion 6 - Economic Growth

Will the completed project enhance economic growth and/or development in the service area?

Definitions:

Secure new employment: The project as designed will secure development/employers, which will immediately add new permanent employees to the junistic tent. The applying agency must submit details.

Permit more development: The project as designed will permit additional business development/employment. The applying agency must supply details.

The project will not impact development: The project will have no impact on business development.

Note: Each project is looked at on an individual basis to determine if any aspects of this category apply.

7) Matching Funds - LOCAL

10 - This project is a loan or credit enhancement

10 – 50% or higher
8 40% to 49.99%
6 – 30% to 39.99%
4 – 20% to 29.99%
2 – 10% to 19.99%

0 - Less than 10%

List total percentage of "Local" funds 47 %

List total percentage of "Local" funds 1/

Criterion 7 - Matching Funds - Local

The percentage of matching funds which come directly from the budget of the applying agency. Ten points shall be awarded if a loan request is at least 50% of the total project cost. (If the applying agency is not a user fee funded agency, any funds to be provided by a user fee generating agency will be considered "Matching Funds – Other").

Matching Funds – OTHER	List total percentage of "Other" funds%			
10 – 50% or higher	List below each funding source and percentage			
8 – 40% to 49.99%	MAF " 3 %"			
6 – 30% to 39.99%				
4 – 20% to 29.99%	<u> </u>			
2 – 10% to 19.99%	<u> </u>			
(1) 1% to 9.99%	<u> </u>			
0 – Less than 1%				

Criterion 8 - Matching Funds - Other

The percentage of matching funds that come from funding sources other than those mentioned in Criterion 7. A letter from the outside funding agency stating their financial participation in the project and the amount of funding is required to receive points. For MRF, a copy of the current application form filed with the Hamilton County Engineer's Office meets the requirement.

9) Will the project alleviate serious capacity problems or hazards or respond to the future level of service needs of the district?

10 - Project design is for future demand.	Appeal Score
8 - Project design is for partial future demand.	• •
6 - Project design is for current demand.	
A- Project design is for minimal increase in capacity.	
(0-)Project design is for no increase in capacity.	

Criterion 9 – Alleviate Capacity Problems

The applying agency shall provide a narrative, along with pertinent support documentation, which describe the existing deficiencies and showing how congestion will be reduced or eliminated and how service will be improved to meet the needs of any expected growth or development. A formal capacity analysis must accompany the application to receive more than 4 points. Projected traffic or demand should be calculated as follows:

Formula:

8)

Existing volume x design year factor = projected volume

<u>Design Year</u>	Design year factor			
	<u>Urban</u>	Suburban	Rural	
20	1.40	1.70	1.60	
10	1.20	1.35	1.30	

Definitions:

Future demand – Project will eliminate existing congestion or deficiencies and will provide sufficient capacity or service for twenty-year projected demand or fully developed area conditions. Justification must be supplied if the area is already largely developed or undevelopable and thus the projection factors used deviate from the above table.

Partial future demand – Project will eliminate existing congestion or deficiencies and will provide sufficient capacity or service for ten-year projected demand or partially developed area conditions. Justification must be supplied if the area is already largely developed or undevelopable and thus the projection factors used deviate from the above table.

<u>Current demand</u> – Project will eliminate existing congestion or deficiencies and will provide sufficient capacity or service only for existing demand and conditions.

Minimal increase – Project will reduce but not eliminate existing congestion or deficiencies and will provide a minimal but less than sufficient increase in existing capacity or service for existing demand and conditions.

 $\underline{\text{No increase}}$ - Project will have no effect on existing congestion or deficiencies and provide no increase in capacity or service for existing demand and conditions.

- 10) Readiness to Proceed If SCIP/LTIP funds are granted, when would the construction contract be awarded?
 - Will be under contract by December 31, 2009 and no delinquent projects in Rounds 20 & 21 3 Will be under contract by March 31, 2010 and/or one delinquent project in Rounds 20 & 21
 - 0 Will not be under contract by March 31, 2010 and/or more than one delinquent project in Rounds 20 & 21

Criterion 10 - Readiness to Proceed

The Support Staff will assign points based on engineering experience and status of design plans. A project is considered delinquent when it has not received a notice to proceed within the time stated on the original application and no time extension has been granted by the OPWC. An applying agency receiving approval for a project and subsequently canceling the same after the bid date on the application will receive zero (0) points under this round and the following round.

11) Does the infrastructure have regional impact? Consider origination and destination of traffic, functional classifications, size of service area, and number of jurisdictions served, etc.

10 – Major Impact	Appeal Score
8 Significant Impact	
6 – Moderate Impact	
4 – Minor Impact	

Criterion 11 - Regional Impact

2 - Minimal or No Impact

The regional significance of the infrastructure that is being repaired or replaced.

Definitions:

Major Impact – Roads: Major Arterial: A direct connector to an Interstate Highway; Arterials are intended to provide a greater degree of mobility rather than land access. Arterials generally convey large traffic volumes for distances greater than one mile. A major arterial is a highway that is of regional importance and is intended to serve beyond the county. It may connect urban centers with one another and/or with outlying communities and employment or shopping centers. A major arterial is intended primarily to serve through traffic.

Significant Impact – Roads: Minor Arterial: A roadway, also serving through traffic, that is similar in function to a major arterial, but operates with lower traffic volumes, serves trips of shorter distances (but still greater than one mile), and may provide a higher degree of property access than do major arterials.

Moderate Impact – Roads: Major Collector: A roadway that provides for traffic movement between local roads/streets and arterials or community-wide activity centers and carries moderate traffic volumes over moderate distances (generally less than one mile). Major collectors may also provide direct access to abutting properties, such as regional shopping centers, large industrial parks, major subdivisions and community-wide recreational facilities, but typically not individual residences. Most major collectors are also county roads and are therefore through streets.

Minor Impact – Roads: Minor Collector: A roadway similar in functions to a major collector but which carries lower traffic volumes over shorter distances and has a higher degree of property access. Minor collectors may serve as main circulation streets within large, residential neighborhoods. Most minor collectors are also township roads and streets and may, or may not, be through streets.

Minimal or No Impact - Roads: Local: A roadway that is primarily intended to provide access to abutting properties. It tends to accommodate lower traffic volumes, serves short trips (generally within neighborhoods), and provides connections preferably only to collector streets rather than arterials.

12)	What is the overall economic health of the jurisdiction?			
	10 Points 8 Points 6 Points 4 Points 2 Points			
	Criterion 12 – Economic Health The District 2 Integrating Committee predetermines the applying agency's economic health. The economic may periodically be adjusted when census and other budgetary data are updated.	c health of a jurisdiction		
13)	Has any formal action by a federal, state, or local government agency resulted in a partial or complete ban of the usage or expansion of the usage for the involved infrastructure?			
	10 - Complete ban, facility closed 8 - 80% reduction in legal load or 4-wheeled vehicles only 7 - Moratorium on future development, not functioning for current demand 6 - 60% reduction in legal load 5 - Moratorium on future development, functioning for current demand 4 - 40% reduction in legal load 2 - 20% reduction in legal load 0 - Less than 20% reduction in legal load Criterion 13 - Ban The applying agency shall provide documentation to show that a facility ban or moratorium has been form moratorium must have been caused by a structural or operational problem. Points will only be awarded in will cause the ban to be lifted.	Appeal Score nally placed. The ban or f the end result of the project		
14)	What is the total number of existing daily users that will benefit as a result of the proposed project?			
•	10 - 30,000 or more 8 - 21,000 to 29,999 6 - 12,000 to 20,999 4 - 3,000 to 11,999 2 - 2,999 and under			
	Criterion 14 - Users The applying agency shall provide documentation. A registered professional engineer or the applying age appropriate documentation. Documentation may include current traffic counts, households served, when of persons. Public transit users are permitted to be counted for the roads and bridges, but only when cer provided.	converted to a measurement		
15)	Has the applying agency enacted the optional \$5 license plate fee, an infrastructure levy, a user fee, or dedicated tax for the pertinent infrastructure? (Provide documentation of which fees have been enacted.)			
	5 - Two or more of the above 3 One of the above 0 - None of the above	Appeal Score		
	on 15 - Fees, Levies, Etc. olying agency shall document (in the "Additional Support Information" form) which type of fees, levies o	r taxes they have dedicated		

b toward the type of infrastructure being applied for.

REPORT OF PAVEMENT EVALUATION STUDY KENWOOD ROAD AND SHAWNEE RUN ROAD MADEIRA, OHIO

FOR

CITY OF MADEIRA HAMILTON COUNTY, OHIO

SEPTEMBER 2007



GEOTECHNICAL, ENVIRONMENTAL AND TESTING: ENGINEERS SINCE 1921

CORPORATE CENTER 611 LUNKEN PARK DRIVE CINCINNATI, OHIO 45226 (513) 321-5816 FAX (513) 321-0294

September 20, 2007 W.O. # 01933.016

Mr. Thomas W. Moeller City of Madeira 7141 Miami Avenue Cincinnati, Ohio 45243

> Re: Report of Pavement Evaluation Study Kenwood Road and Shawnee Run Road City of Madeira, Hamilton County, Ohio

Dear Mr. Brandstetter:

The H.C. Nutting Company is pleased to submit our report of Pavement Evaluation along Shawnee Run Road and preliminary pavement evaluation along Kenwood Road in the City of Madeira, Ohio. Our services were performed in general accordance with our proposal dated August 21, 2007 and consultant agreement/authorization by City of Madeira on August 22, 2007.

The work performed for this pavement evaluation consisted of: (1) test boring layout in the field, (2) drilling of eleven shallow test borings in the existing roadway, (3) laboratory testing and engineering analyses, and (4) preparation of this report. The following paragraphs summarize a description of the project, our investigative procedures, the encountered subsurface conditions, geotechnical recommendations for roadway and subgrade improvements as necessary. An information sheet describing the basis and limitations of this study follows the text. Figures, test boring logs, summary of laboratory test data, and information describing the terminology used on the boring logs and laboratory data sheets are included in the Appendix of this report.

It should be noted that only three widely spaced borings were drilled along Kenwood Road. Therefore, the provided recommendations for remediation of Kenwood Road should be considered preliminary.

We appreciate this opportunity of providing these geotechnical services for you. Should you have any questions concerning the contents of this report or if we may be of service during construction, please contact us.

Thank you for your consideration.

Respectfully submitted,
H. C. NUTTING COMPANY

Bobby Daita, E.I.

Staff Geotechnical Engineer

Śwaminathan Srinivasan, P.E. Senior Principal/Chief Engineer

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SOIL CLASSIFICATION

FIGURE 1: SITE VICINITY MAP

FIGURE 2: TEST BORING LOCATION PLAN

TEST BORING LOGS

TABLE I: SUMMARY OF LABORATORY TEST DATA

TABLE II: TABULATION OF UNDISTURBED DATA

SAMPLE DISPOSITION

1.0 INTRODUCTION

The H. C. Nutting Company (HCN) was retained by City of Madeira to perform Pavement Evaluation along Shawnee Run Road and preliminary pavement evaluation along Kenwood Road in Madeira, Ohio. This evaluation generally describes the existing pavement and pavement subgrade soils conditions and provides recommendations for potential remediation. The scope of our study includes a subsurface exploration consisting of 11 soil test borings (3 along Kenwood Road and 8 along Shawnee Run Road), visual classification, and laboratory testing of representative soil samples, geotechnical engineering analyses and preparation of this report.

This geotechnical report provides a summary of our site reconnaissance, existing pavement and subgrade conditions, recommendations for general site development and subgrade remediation as it pertains to the proposed roadway improvements. The Appendix of this report also includes a Site Vicinity Map (Figure 1), Test Boring Location Plan (Figure 2), test boring logs, and laboratory test results (Table 1 & 2). Also included in the Appendix are descriptions of terminology used in the test boring logs, important information regarding the basis and limitations of this study, and a form regarding the disposition of the acquired samples.

2.0 PROJECT DESCRIPTION

The project consists of evaluating the existing pavement and subgrade profile along portions of Kenwood Road and Shawnee Run Road in Madeira, Ohio. The proposed evaluation along Kenwood is approximately 3,000 ft., between Dawson Avenue and Euclid Avenue. The pavement evaluation along Shawnee Run Road is approximately 5,350 ft. between Kenwood Road and Miami Avenue. The general location and project limits along Kenwood Road and Shawnee Run Road are depicted on Figure 1 Site Vicinity Map. The pavement study along Kenwood road is considered preliminary due to the widely-spaced (approximately 1,000 ft. apart) borings.

Kenwood Road runs in a general north-south direction and has a rolling topography. Pavement distress along Kenwood Road was less frequent in comparison to Shawnee

Run Road. Based on the Typical Section Sheet for the widening of Kenwood Road that was completed by the Hamilton County Engineers Office in 1949, the original 20 ft. wide concrete pavement was widened 8.5 ft. on either side using Class D concrete and the improved pavement was covered with 1 inch thick bitumen binder course and 1 inch thick bitumen concrete surface course. The widened sections also contained a Type "A" mesh fabric sandwiched between concrete pavement and bitumen binder course.

Shawnee Run Road runs in an east-west direction between Kenwood Road and Miami Road with a small portion of its alignment in north-south direction. The alignment of Shawnee Run Road between these roads can be divided into three sections based on their topography — Section I between Kenwood Road and portion of the road in north-south direction has a rolling topography, Section II between the portion where the road continues back in a east-west direction to its intersection with Camargo Road has a downslope topography, and Section III between Camargo Road and Miami Road has an upslope topography. Section II and Section III showed frequent pavement distress features in comparison with Section I.

The existing pavement along Kenwood Road and Shawnee Run Road consist of isolated areas which have undergone distress. Based on our visual observations, the majority of pavement distress consists of longitudinal and transverse cracking, and some alligator cracking. Occasional potholes and/or depressions were observed along Kenwood Road and Shawnee Run Road. "Troughing" within the wheel paths was also observed along Shawnee Run Road. Both Kenwood Road and Shawnee Run Road showed indications of pavement patching due to installation of utilities along the length of the road on both sides of the pavement. In general, the existing pavement along Shawnee Run Road exhibited more widespread distress as a result of subgrade deterioration. The existing pavement along Kenwood Road and Shawnee Run Road shows features of pavement patching performed subsequent to utility installation along the roadway alignment. Details regarding the backfilling of utility excavation and pavement patching were not reviewed.

The project description information was based on our site reconnaissance, the information provided, and review of the available project plans provided by Brandstetter

Carroll, Inc. If any of the above information needs modification, please notify H. C. Nutting so that we may review our recommendations and provide any necessary changes.

3.0 FIELD EXPLORATION AND LABORATORY TESTING

3.1 Field Exploration

A total of 11 shallow soil test borings were drilled for this geotechnical study for the evaluation of the existing pavement and subgrade soils. The test boring locations were located in the field by HCN personnel. Test borings K-1, K-2 and K-3 were drilled along Kenwood road between Dawson Avenue and Euclid Avenue and test borings P-1 to P-8 were drilled along Shawnee Run Road between Kenwood Road and Miami Avenue. Test borings along Kenwood Road were approximately 1,000 ft. apart and those on Shawnee Run Road were approximately 500 to 700 ft. apart. The test boring locations included a combination of areas with and without distress. The approximate locations of the test borings are illustrated on Figure 2, Test Boring Location Plan, in the Appendix of this report. The following table summarizes the location of test boring with respect to the nearest street address.

Test Boring Locations

rest borning Locations					
Boring	Lane	Nearest House			
K-1	Southbound	6929 Kenwood Road			
K-2	Northbound	6830 Kenwood Road			
K-3	Northbound	6662 Kenwood Road			
P-1	Eastbound	6506 Shawnee Run Road			
P-2	Westbound	6715 Shawnee Run Road			
P-3	Eastbound	6941Shawnee Run Road			
P_4	Westbound	7137 Shawnee Run Road			
P-5	Eastbound	7361 Shawnee Run Road			
P-6	Eastbound	7561Shawnee Run Road			
P-7	Westbound	Near Miami Avenue			
P-8	Westbound	7200 Shawnee Run Road			

The test borings were drilled between August 30 and September 4, 2007 using truck mounted rotary drilling equipment. Traffic control was necessary to access and drill the test borings and was provided by the City of Madeira.

Pavement cores were obtained at each test boring location and the thickness of granular base was noted to the nearest 1/4th of an inch. Boreholes were then advanced and stabilized using hollow-stem augers and Shelby tube samples (in accordance with ASTM D 1587) of the subgrade soils immediately below the pavement section and granular base were obtained at each of the test boring locations. Continuous sampling was then accomplished using the Standard Penetration Test procedure (ASTM D 1586). This procedure involves driving a 2 inch O.D. by 1 ¾ inch I.D. split-spoon sampler with a 140 lb. hammer falling 30 inches. The number of blows required for each 6 inches of penetration is recorded; the Standard Penetration Test result, or N-value, is the number of blows for the final 12 inches of penetration within each driving interval. These "split-spoon" samples were obtained continuously to the boring termination depth. Test borings extended to depths of about 6.3 to 7.5 feet below existing site grades. All soil samples were stored in air-tight jars to preserve moisture and integrity.

Four representative bag samples (SB-1 to SB-4) were obtained within the upper 3 ft. of subgrade soils near the test borings as described in the following table.

Bag Samples

Nearest Borings
. K-1,K-2, K-3
P-1, P-2, P-3
P-5, P-6, P-7
P-4, P-8

Upon completion of the drilling activities, the boreholes were backfilled with the drill cuttings and patched at the existing roadway surface. Groundwater levels were observed during and at completion of the drilling activities. Since the boreholes were backfilled immediately upon completion for safety reasons, long-term (24-hour) water levels were not obtained for this project.

3.2 Laboratory Testing

Upon completion of drilling operations, all samples were returned to our Soil Mechanics Laboratory. Each sample was examined and visually classified by the project geotechnical engineer in accordance with the USCS Soil Classification System. Laboratory tests consisting of natural moisture content determinations were performed on the obtained split-spoon samples. In situ unit weight determinations were performed on obtained Shelby tube samples. Atterberg Limits test (3-point) was performed on selected Shelby tube and bag samples. Standard Proctor test was performed on three bag samples.

The test boring logs were reclassified by the project geotechnical engineer based on the drill foreman's field notes, the laboratory examination of the recovered samples, and the results of the laboratory tests. The reclassified test boring logs are included in the Appendix.

4.0 ENCOUNTERED SUBSURFACE CONDITIONS

The test borings generally encountered asphalt pavement and concrete pavement underlain by granular base or broken concrete at surface. Existing fill soils and natural overburden cohesive soils were encountered below the surficial material to the explored test boring depths. The following paragraphs provide a brief description of the encountered subsurface conditions in order of increasing depth below existing grade.

4.1 Surficial Materials

The surficial materials at the test boring locations generally consisted of asphalt pavement and concrete pavement (along Kenwood Road) underlain by granular base or broken concrete. The granular base consisted of crushed limestone, with sand or sand and gravel.

Along Kenwood Road the thickness of asphalt pavement varied between 2.75 and 10 inches. At test borings K-2 and K-3, 7.5 inches thick concrete pavement with a

reinforcing mesh (1/4" bars both ways) was encountered beneath the asphalt pavement. Granular base with thickness varying between 4 and 8 inches was encountered below the asphalt pavement at test borings K-1 and K-2

Along Shawnee Run Road, the thickness of asphalt pavement varied between 6 and 17 inches. Concrete pavement encountered at boring P-8 was 8.5 inches thick. Below the asphalt pavement, broken or crushed concrete was reported at test borings P-1, P-2, P-3, and P-5 and granular base was reported at test borings P-4, P-6, P-7, and P-8. The thickness of broken concrete varied between 5 and 13 inches and that of granular base varied between 8 and 18 inches.

The following table summarizes the thickness of asphalt pavement and underlying granular base/concrete.

Surficial Conditions at Test Borings

Carnotal Collations at Test Dollings						
Test Boring	Asphalt Pavement Thickness (in.)	Concrete Pavement Thickness (in.)	Base Material	Base Material Thickness (in.)		
K-1	10	NE	Granular Base	8		
K-2	5 (2½ + 2½)	. 71/2	Granular Base	3		
K-3 .	2 3/4	7 1/4	NE	NE		
P-1	9 1/4 (11/4 +21/2 +51/2)	NE	Broken Concrete	7		
P-2	6 (1+ 2 ½ +2 ½)	NE	Broken Concrete	11		
P-3	17 (2½ +2 ½+2 ½+9 ½)	NE	Broken Concrete	13		
P-4	9	NE	Granular Base	8		
P-5	101⁄2	NE	Broken Concrete	5		
P-6	8½ (1¼+3¾+3½)	81/2	Granular Base	10		
P-7	7 (3 ½+ 3 ½)	NE	Granular Base	18		
P-8	7	NE	Granular Base	10		

NE: Not Encountered

4.2 Existing Fill

Along Kenwood Road existing fill was encountered at all of the test borings below the surficial material and extended to depths of about 3.5 to 5.5 ft. below existing grades. The encountered fill was visually classified as lean clay and clay and contained variable amounts of sand and gravel. Based on pocket penetrometer readings (an approximation of unconfined compression strength) that varied between 1.5 and 4 tsf,

the encountered fill was stiff to very stiff in consistency. Laboratory tested natural moisture contents of existing fill soils varied between 18% and 29%.

Along Shawnee Run Road, existing fill was encountered below surficial material at test borings P-2, P-3, P-4, and P-6 and extended to depths of about 3.4 to 6.3 ft. below existing grades. The following table summarizes the depth and thickness of the encountered existing fill.

Encountered Fill Thickness

Test Boring	Fill Thickness (ft.)	Bottom of Fill Depth (ft.)
K-1	4	5,5
K-2	2.3	3.5
K-3	2.7	3.5
P-2	2 .	3.4
P-3	2	4.5
P-4 .	3.6	5
P-6	4.9	6.3*

^{*-}Boring was terminated in possible fill material

The encountered fill at borings drilled along Shawnee Run Road was predominantly cohesive and was visually classified as silty clay, lean clay, and clay and contained variable amounts of sand, gravel, shale and limestone fragments. The encountered fill was soft to stiff in consistency with recorded pocket penetrometer reading values varying between 0.5 and 2 tsf. SPT N-values of cohesive fill soils varied between 7 and 59 blows per foot (bpf). Granular fill encountered at boring P-6 was visually classified as gravel and cobbles and clayey sand and gravel. The granular fill was loose to medium dense based on the compactness of the Shelby tube sample and SPT N-value of 14 bpf. Laboratory tested natural moisture contents of fill soils varied between 15% and 30%. Atterberg Limits tests performed on a Shelby tube sample of existing fill showed Liquid Limit and Plasticity Index of 26 and 5, respectively.

The encountered fill along both Kenwood Road and Shawnee Run Road was variable in consistency/compactness and we have not reviewed any records showing that the fill was placed and compacted in a controlled manner.

4.3 Natural Overburden Soils

Beneath the existing fill or surface material natural overburden cohesive and granular soils were encountered at all of the test borings except P-6. The encountered cohesive soils were of glacial and residual origin. Glacial till is an unsorted, unstratified mixture of silt, sand, gravel, and clay which was deposited discontinuously by glacial ice moving over bedrock or older glacial deposits. Residual soils are derived from complete decomposition or weathering of the parent rock. Residual clays encountered at the borings were from complete decomposition of shale bedrock. The encountered granular soils were of glacial outwash origin.

Along Kenwood Road, the encountered cohesive soils were visually classified as lean clay, clay, and fat clay and contained variable amounts of sand and limestone fragments. All three test borings were terminated within natural cohesive soils at a depth of 6.5 ft. The encountered cohesive soils were soft to very stiff in consistency with recorded pocket penetrometer readings varying between 1 and 4 tsf. SPT N-values of cohesive soils varied between 2 and greater than 50 bpf. The higher blows counts can be attributed to the presence of limestone fragments.— Some of the samples with high blow counts were very moist to wet resulting in a soft consistency. Laboratory tested natural moisture contents of natural cohesive soils encountered at test borings along Kenwood Road varied between 18% and 25%.

All the test borings along Shawnee Run Road except boring P-6 were terminated within natural overburden soils. Natural overburden soils encountered along Shawnee Run Road were predominantly cohesive in nature and were visually classified as lean clay, clay, and fat clay and contained variable amounts of sand and limestone fragments. The encountered natural cohesive soils were medium stiff to very stiff based on pocket penetrometer readings that varied between 1 and 4 tsf. SPT N-values of natural cohesive soils varied between 8 bpf and greater than 50 bpf with the higher blows counts possibly due to the presence of limestone fragments within the residual clays. Laboratory tested natural moisture contents of natural cohesive soils encountered at test borings along Shawnee Run Road varied between 17% and 30%. Atterberg Limits

tests performed on Shelby tube sample of natural cohesive soils obtained at P-5 showed Liquid Limit and Plasticity Index of 32 and 16, respectively.

Natural granular soil visually classified as clayey sand was encountered at test boring P-1 from depths of 3.4 ft. to the boring termination depth of 6.4 ft. The encountered clayey sand was wet and based on a SPT N-value of 18 bpf medium dense in compactness.

4.4 Groundwater

Groundwater observations were made at all the test boring locations during and upon completion of drilling the test borings. The boreholes were immediately backfilled with auger cuttings following the removal of augers and patched at the roadway surface for safety considerations.

Along Kenwood Road, groundwater was encountered during drilling at test borings K-1 and K-3 at depths of about 5.5 ft. and 5 ft. respectively. No water or "dry" conditions were reported at all the three test borings upon completion of drilling operations.

During and upon completion of drilling, water was not encountered at any of the test borings drilled along Shawnee Run Road and no water or "dry" conditions were reported. However, some of the obtained Shelby tube samples showed zones of wet soils due to perched water. A "dry" condition is reported when no water is observed in the open borehole or on the sampling tools.

The groundwater observations are often not representative of the actual groundwater conditions since the boreholes are left open for a relatively short period of time groundwater levels will vary based on seasonal conditions, surface runoff, evaporation, precipitation, and other related hydrogeologic factors. Furthermore, trapped or perched water is often encountered within the existing fill and/or at the fill/natural interface. Based on the encountered conditions at our test borings, we anticipate that wet subgrade conditions due to perched water in fill might be encountered beneath the existing asphalt pavement and granular base.

5.0 CONCLUSIONS AND RECOMMENDATIONS

5.1 Pavement and Subgrade Evaluation

Pavement design is a function of several variables including subgrade strength, drainage, traffic type and volume, amount of truck traffic, and reasonable levels of statistical reliability. Based on these factors, a structural number (SN) is determined, which is in turn used to calculate a pavement section that will satisfy the design parameters. We have not reviewed the pavement design for Kenwood and Shawnee Run Roads; however, based on our understanding of pavement design and experience, we believe that the distress observed is a combination of marginal/poor subgrade conditions and an insufficient design pavement section. The observed distress is likely the result of several attributing factors. Based on our site reconnaissance, and test boring and laboratory results, we offer the following discussion outlining the most likely causes of the observed pavement distress.

Based on the encountered conditions in the test borings performed for this study, the existing pavement section and base material is variable. Pavement thickness varied between 23/4 and 17 inches and base material varied between 3 and 8 inches. In addition to the variable thickness, the pavement and base material types also varied. Both asphalt and mesh reinforced concrete pavement sections were encountered. Base material consisted of both granular aggregate and broken/degraded concrete. Variations in type and thickness could be related to construction methods, dissimilar repair and replacement methods, and/or dissimilar replacement methods following underground utility installation. Each of the variations of pavement/base course type and thickness will result in a variety of structural numbers, some of which do not satisfy traffic loading/volume conditions.

Although the encountered pavement may have been initially adequately designed, traffic volume, percentage of trucks, and projected growth may have been exceeded the design assumptions and projections. A typical pavement design life is 20 years. We have not reviewed as-built documents, but it could be that the design life of the

pavement has been exceeded. Individually or in combination, an insufficient initial design and/or exceeded pavement life could result in the observed pavement distress.

Insufficient compaction of soils following underground utility installation can also lead to distress within the pavement. Utility trench type patterns were observed along Kenwood Road, which indicate differential settlement between the utility and surrounding pavement areas. Backfill soils not properly placed and/or minimal pavement replacement will result in distress at the pavement surface.

Based on the pavement section described on Hamilton County Engineers 1949 drawings for Kenwood Road, concrete pavement was utilized and has since been overlain with asphalt. However, we only encountered concrete in two of the three widely-spaced test borings performed along Kenwood Road. Variable pavement types will respond and wear differently to the traffic loading. If not properly "jointed", longitudinal cracking along the joints of the different types will develop.

The alligator, ruts, and deflections observed along the roadways indicate that the underlying subgrade soils are not providing sufficient support to the pavement section. Distress within the subgrade reflects up into the pavement. Consequently, without proper attention to the subgrade soils, pavement distress also reflects through the repaired sections. The subgrade distress is attributed to fatigue over time, poor drainage and subsequent seasonal cycles of freeze/thaw, which results in seasonal volume change within the subgrade soils.

Although the above reasons have all likely attributed to the observed pavement distress and failure along Kenwood and Shawnee Run Roads, deterioration to the subgrade soils is likely the primary attributor. The subgrade conditions are further discussed below.

Kenwood Road

The subgrade soils along Kenwood Road generally consisted of moderately plastic cohesive existing fill soils. Standard Proctor test performed on a bag sample obtained between depths of 1 and 3 ft. near test borings K-1, K-2, and K-3 showed Maximum Dry

Density (γ_{dmax}) and Optimum Moisture Content (OMC) of 109.5 pcf and 16.9%. Atterberg Limits tests performed on the bag sample showed Liquid Limit and Plasticity Index of 37 and 19, respectively. A comparison of the in situ dry unit weights and natural moisture contents against Standard Proctor results is provided in the following table.

In situ Moisture and Density Data Along Kenwood Road

Test Boring	In situ Moisture (%)	Δ OMC (%)	Dry Unit Weight (pcf)	Δγ _{dmax} (pcf)	(γ _d /γ _{dmax})%
K-1	26	+9.1	97.7	-11.8	89
K-2	29	+12.1	95.7	-13.8	87
K-3	18	+1.1	104.6	-4.9	96

In general, pavement subgrades should be compacted to 98% to 100% of maximum dry unit weight at moisture contents within ±3% of optimum moisture content. The upper 12" of the subgrade soil should be compacted to 100% Standard Proctor maximum dry density. From the table, the existing subgrade soils are generally wet of optimum with in situ moisture contents as high as 12% greater than OMC. The dry unit weights of the in situ soils is lower than the maximum dry unit. Pavement subgrades compacted wet of optimum at low dry unit weights will result in long-term settlement and shear failure of the subgrade which emerge to the pavement surface as ruts and other distress patterns.

Shawnee Run Road

The subgrade soils beneath the surficial pavement consisted of either existing fill or natural cohesive soils. Standard Proctor test performed two bag samples obtained between depths of 1 and 3 ft. near test borings P-1, P-2, and P-3 (SB-2) and near test borings P-5, P-6, P-7 (SB-3) showed Maximum Dry Density (γ_{dmax}) and Optimum Moisture Content (OMC) of 108.6 pcf and 16.7% and 107.2 and 18.6%, respectively. Atterberg Limits tests performed on bag samples SB-2 and SB-3 showed Liquid Limit and Plasticity Index of 33 and 16, and 39 and 121, respectively. The following table compares the in situ dry unit weights and natural moisture contents against Standard Proctor results.

In situ Moisture and Density Data Along Shawnee Run Road

民族政治和政治	In situ		Dry Unit	DEPOSIT DE LE	BY SHAREST NO. 12 P. P.
Test Boring	Moisture. (%)	Δ OMC (%)	Weight (pcf)	Δ γ _{dmax} (pcf)	(Yd /Ydmax)%
P-1	23.9	+7.2	99.8	-8,8	92
P-2	24.1	+7.4	120.5	+11.9	111
P-3 NA		NA	NA	NA	NA
P-4	18.9	+2.2	103.8	-4.8	96
P-5	24.8	+6.2	101.7	-5.5	95
P-6	NA	NA	NA	NA	NA
P-7	23.5	+4.9	101.3	-5.9	94
P-8	34.1*	+17.4	69.1*	39.5	64

NA-Not Available due to zero recovery in Shelby tube *-the sample was organic

The cohesive soil encountered at the pavement subgrade level at test boring P-8 contained organics. The tested moisture content was high and the unit weight was low due to the presence of organics. The presence and extent of organics in the vicinity of test boring P-8 should be further evaluated in the field during construction.

The in situ moisture contents of the subgrade soils were generally 2 to 17% greater than the OMC in comparison to the required $\pm 3\%$ OMC range. Also, in situ dry unit weights were generally low (between 92 and 96%) in comparison to the required 98 to 100% of γ_{dmax} . The subgrade soils are not at the desired levels of moisture content and dry unit weight requirements for adequate performance of pavement.

5.2 Pavement and Subgrade Remediation

Based on our site reconnaissance, it appears that Kenwood Road and Shawnee Run Road were excavated for various utility installations. These excavations were backfilled and the pavement was patched. However, the backfill was probably not likely adequately compacted as structural fill and the patched pavement section was probably not equivalent to the original pavement section. In addition, poor drainage provisions have resulted in zones of wet subgrade soils with perched water. It is our opinion that the current pavement distress is a result of a variable and often insufficient pavement section underlain by subgrade soils which are wet of optimum with low dry unit weights. Additionally, insufficient and improper drainage provisions might have resulted in

pavement distress. The effects of poor subgrade conditions will be reflected on an asphalt overlay over the existing pavement in the form of distress. Therefore, remedial measures should result in a new pavement section that will be supported on well compacted and controlled structural fill. A new pavement section with appropriate drainage provisions designed for the anticipated traffic loads should be used for repaving over the structural fill subgrade.

The upper 2 ft. of pavement subgrade soils should be reworked and recompacted as structural fill. The encountered fill soils at test borings are suitable for reuse as structural fill provided they are moisture conditioned to near OMC moisture contents. Moisture conditioning can be achieved by discing and drying. However, based on the time of year of construction and project schedule, discing and drying of the subgrade soils may not be the most efficient method. Alternative subgrade improvement methods like chemical modification and geogrid and stone stabilization can also be considered. Recommendations for structural fill placement, chemical modification, and geogrid stabilization are provided in the following paragraphs.



5.3 Site Preparation & Structural Fill Placement

Site preparation should begin with stripping of asphalt pavement and granular base. The stripping, clearing, and grubbing procedures should be performed in accordance with current ODOT construction specifications. The granular base can be reused during repaving operations. The concrete encountered should be adequately broken to the size of allowable granular base material size. The processed concrete can be used as a fill material but is not suitable for use as a granular base below pavement section. It is anticipated that existing fill or natural cohesive soils will be encountered at the subgrade level upon performing this initial site preparation.

Following clearing, grubbing, stripping of existing surficial material, and removal of construction debris we recommend a 2 ft. undercut of the subgrade soils. The exposed soils upon performing the undercut operation should proofrolled prior to the placement of new structural fill. The proofroll should be performed with several passes of heavy construction equipment, such as a minimum 20-ton loaded tandem axle dump truck or

heavy-duty sheepsfoot roller. These operations will delineate any areas which yield, rut, or pump that may require further undercutting or other stabilizing methods. We recommend that a geotechnical field representative observe proofrolling and subgrade preparation so that they may evaluate the subgrade soils suitability and adequacy and determine if any additional undercut is required.

The undercut subgrade should be backfilled with new structural fill. The undercut soils can be reused as structural fill provided they are subjected to moisture conditioning. Cohesive fill soils with organics were encountered at boring P-8. Any such soils if encountered should be blended with other soils such that organic content of the final product is less than 4%. Based on our test borings, the subgrade soils were generally wet of optimum. Moisture conditioning can be performed by discing and drying the undercut soil. It is important to note this work should be performed when long periods of dry, warm weather are forecast. The subgrade remediation can also be achieved by chemical modification or with the use of geogrid and stone; details of which are provided in the following section. Any proposed borrow source for structural fill should be evaluated by the project geotechnical engineer prior to trucking to the site.

Structural fill should be placed in general accordance—with current specifications. Material used as structural fill should be free of organic material (less than about 4 percent), vegetation, or other deleterious substances. All fill required in structural areas (beneath the roadway footprint and at least 18 inches beyond the proposed edge of pavement) should be compacted to at least 98 percent Standard Proctor maximum dry density (ASTM D 698). The upper 1 foot of the pavement subgrade should be compacted to at least 100 percent of the Standard Proctor density. Cohesive and granular type fill material can be placed in maximum 8 inch loose, horizontal lifts prior to compaction, provided heavy-duty, self-propelled compactors are used. For small or confined areas, or where small walk behind rollers, plate compactors, or tampers are used, loose lift thicknesses should be limited to 4 to 6 inches.

Ideally, the fill material should have a liquid limit of less than 40 and contain fragments less than 4 inches in maximum dimension. The use of the moderately higher plasticity clay (liquid limit greater than 40) as structural fill in the upper foot of the subgrade

should be avoided. Each fill lift should be brought within a moisture content range of approximately 3 percent of its optimum moisture content. Each fill lift should be compacted, tested by geotechnical personnel and approved, prior to placing any subsequent fill.

5.4 Subgrade Treatment

As mentioned earlier, the undercut soils can be reused as structural fill provided they are subjected to moisture conditioning or stabilized. Chemical modification and geogrid stabilization are two alternative methods that can be adopted to rework the subgrade soils to make them suitable for reuse as structural fill.

Geogrid Stabilization

The geogrid stabilization option requires the roadway subgrade soil be undercut or established a minimum of 18" (in three lifts) below the proposed subgrade elevation. A layer of Tensar BX-1200 geogrid should be placed directly on the soil subgrade, and then a minimum 18" of granular base course of crushed limestone (No. 53 stone) should be placed directly over the geogrid. Consideration may also be given to "punching" a layer of No. 2 stone into the subgrade to provide additional support and a capillary break. Then the layer of geogrid may be placed on top of the No. 2 stone, and the 18" of granular base course of crushed limestone should be placed directly over the geogrid. The granular base course of crushed limestone should be placed in three, six-inch compacted lifts, compacted to at least 98% Standard Proctor Density.

Chemical Modification

The upper 16" of the exposed subgrade soils can be subjected to in-place chemical modification to create a firm subgrade. Chemical modification will dry/stabilize the soil and will provide more 'weather protection' for the exposed subgrade than untreated soil. To properly realize the benefits that are produced when chemically modifying soils, proper construction techniques must be utilized by a specialty contractor. Lime is often used to modify clay soils; however, due to the low plasticity of the on-site soils, cement or a lime-cement mixture may be more beneficial. This modification work should be done on a performance-specification basis. The actual lime/cement percentage added may vary and will likely involve some experimentation. It is for this reason that we

strongly suggest using a subcontractor who is experienced in lime/cement modification to perform the work. Typically for drying purposes, it has been our experience to use approximately 3% to 4% lime or cement per dry unit weight of the soils to modify the soils to within optimum moisture content.

5.5 Pavement Design Considerations

Following pavement subgrade preparation by reusing the existing fill as structural fill upon moisture condition in accordance with our recommendations design of asphaltic concrete pavement can be based on a CBR value of 4 and a resilient modulus of 4800 psi. Higher CBR value of 6 can be used for pavement subgrade modified following geogrid stabilization or chemically modified subgrade soils. For rigid concrete pavement, a modulus of subgrade reaction of 125 pci can be used for the design. Again, if the pavement subgrade is stabilized with geogrid or lime/cement modified, a modulus of subgrade reaction of 150 pci can be used.

Proper drainage of the pavement subgrade will extend pavement life. The new pavement section should include a granular base below the asphalt pavement. Sloping or crowning the new subgrade should be considered for positive drainage. Additionally, surface water runoff from areas adjacent to and sloping towards the pavement should be intercepted, collected and not permitted to flow onto the pavement or infiltrate the pavement base and subgrade material. The control and disposal of surface and subsurface water is a very important part of pavement design. It is our opinion that the existing pavement problems are most probably caused by prolonged retention of water on the surface and within or beneath the pavement. Therefore, a drainage ditch or edge underdrain should be considered to intercept seepage and water moving down the subgrade slope.

6.0 CONSTRUCTION AND QUALITY CONTROL CONSIDERATIONS

It is recommended that all aspects of this roadway reconstruction be performed in accordance with the current ODOT standards. It is recommended that testing and inspection by qualified geotechnical personnel be utilized during the construction phase of the project. These services should be performed during proof rolling activities, undercutting and placement of any structural fill and reconstruction of pavement. We request the opportunity of remaining involved with the project through the construction phase by providing materials testing and monitoring services. Testing and inspection is considered essential to evaluate site and construction conditions as they relate to these findings and recommendations.

The test borings along Kenwood Road were widely spaced and hence the recommendations provided for Kenwood Road should be considered preliminary. A final pavement evaluation study with more closely-spaced test borings is recommended.

LIMITATIONS OF LIABILITY

OUR WARRANTY

We warrant that the services performed by H. C. Nutting Company are conducted in a manner consistent with that level of care and skill ordinarily exercised by members of the profession currently practicing under similar conditions NO OTHER WARRANTIES, EXPRESSED OR IMPLIED, ARE MADE. While the services of H. C. Nutting Company are a valuable and integral part of the design and construction teams, we do not warrant, quarantee, or insure the quality or completeness of services provided by other members of those teams, the quality, completeness, or satisfactory performance of construction plans and specifications which we have not prepared, nor the ultimate performance of building site materials.

SUBSURFACE EXPLORATION

Subsurface exploration is normally accomplished by test borings; test pits are sometimes employed. The method of determining the boring location and the surface elevation at the boring is noted in the report. The information is represented on a drawing or on the boring log. The location and elevation of the boring should be considered accurate only to the degree inherent with the method used.

The boring log includes sampling information, description of the materials recovered, approximate depth of boundaries between soil and rock strata and groundwater data. The log represents conditions specifically at the location and time the boring was made. The boundaries between different soil strata are indicated at specific depths; however, these depths are in fact approximate and dependent upon the frequency of sampling. The transition between soil strata is often gradual. Water level readings are made at the times and under the conditions stated on the boring logs. Water levels change with time and season. The borehole does not always remain open sufficiently long for the measured water level to coincide with the groundwater table.

LABORATORY AND FIELD TESTS

Tests are performed in accordance with specific ASTM Standards unless otherwise indicated. determinations included in a given ASTM Standard are not always required and performed. Each test report indicates the measurements and determinations actually made.

ANALYSIS AND RECOMMENDATIONS

- The geotechnical report is prepared primarily to aid in
- the design of site work and structural foundations.
- Although the information in the report is expected to
- be sufficient for these purposes, it is not intended to
- determine the cost of construction or to stand alone as a construction specification.

Report recommendations are based primarily on data from test borings made at the test locations shown on a boring location drawing included. Soil variations

- may exist between borings and these variations may not become evident until construction. If significant
- variations are then noted, the geotechnical engineer
- should be contacted so that field conditions can be
- examined and recommendations revised if necessary.
- The geotechnical report states our understanding as to the location, dimensions and structural features
- proposed for the site. Any significant changes in the
- nature, design, or location of the site improvements
- MUST be communicated to the geotechnical engineer
- so that the geotechnical analysis, conclusions, and recommendations can be appropriately adjusted.
- The geotechnical engineer should be given the opportunity to review all drawings that have been prepared based on his recommendations.

CONSTRUCTION MONITORING

- Construction monitoring is a vital element of complete
- geotechnical services. The field engineer/inspector is
- the owner's "representative" observing the work of the
- contractor, performing tests as required in the
- specifications, and reporting data developed from
- such tests and observations. THE FIELD ENGINEER
- OR INSPECTOR DOES NOT DIRECT
- **CONTRACTOR'S** CONSTRUCTION MEANS.
- METHODS, OPERATIONS OR PERSONNEL. He
- does not interfere with the relationship between the
- owner and the contractor and, except as an observer,
- does not become a substitute owner on site. He is
- responsible for his own safety but has no
- responsibility for the safety of other personnel at the
- site. He is an important member of a team whose
- responsibility is to watch and test the work being done and report to the owner whether that work is being
- carried out in general conformance with the plans and
- specifications.

APPENDIX

BORING TERMINOLOGY SOIL CLASSIFICATION

FIGURE 1: SITE VICINITY MAP

FIGURE 2: TEST BORING LOCATION PLAN

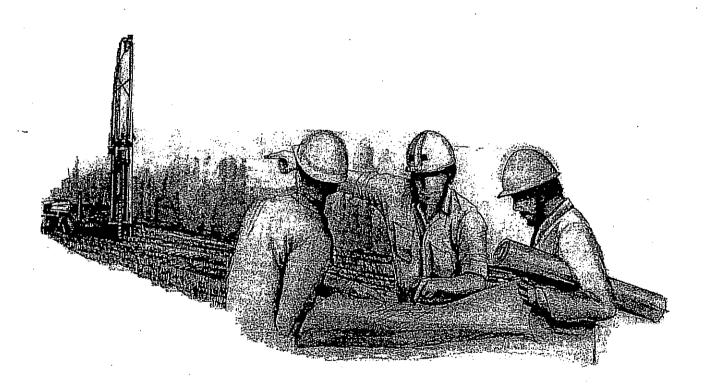
TEST BORING LOGS

TABLE I: SUMMARY OF LABORATORY TEST DATA TABLE II: TABULATION OF UNDISTURBED DATA

SAMPLE DISPOSITION

A description of terminology and symbols used in the logs of test borings, and a copy of ASTM D 2487, "Classification of Soils for Engineering Purposes", are included in the following two pages.

Readers of this report who wish an in-depth discussion on the basis for geotechnics, including procedures used in subsurface exploration, laboratory testing, and geotechnical analyses are referred to The H. C. Nutting Geotechnical and Test Engineering Manual. Those readers not having a copy of this manual may obtain one at nominal cost by contacting The H. C. Nutting Company at (513) 321-5816.



LOG OF TEST BORING: TERMINOLOGY AND SYMBOLS

STANDARD PENETRATION TEST

THE PENETRATION RESISTANCE OR N-VALUE AS IT IS COMMONLY REFERRED TO IS THE SUMMATION OF THE NUMBER OF BLOWS REQUIRED TO DRIVE TWO SUCCESSIVE 6" PENETRATIONS OF THE 2" O.D. SPLIT BARREL SAMPLER. THE SAMPLER IS DRIVEN WITH A 140 LB. WEIGHT FALLING 30" AND IS SEATED TO A DEPTH OF 6' BEFORE COMMENCING THE STANDARD PENETRATION TEST.

THE STANDARD PENETRATION TEST IS PERFORMED IN COMPLIANCE WITH PROCEDURES AS SET FORTH IN ASTM D-1586.

TERMINOLOGY

GRAIN SIZE (PER ASTM D-2487)

SOIL FRACTION		PARTICLE SIZE	U.S. STANDARD SIEVE SIZE
BOULDERS		LARGER THAN 12" (300mm)	LARGER THAN 12"
COBBLES		3' (75 mm) TO 12' (300 mm)	3" TO 12"
GRAVEL:	COARSE	14" (19 mm) TO 3' (75 mm)	W TO 3"
	FINE	4.75 mm TO 19mm	#4 TO 3/2
SAND:	COARSE	2.00 mm TO 4.75 mm	#10 TO #4
	MEDIUM	0.425 mm TO 2.60 mm	#40 TO #10
	FINE.	0.075 mm TO 0.425 mm	#200 TO #40
FINES: PLA	(SILTS & CLAYS) STICITY CHARACTERIS	SMALLER THAN 0.075 mm STICS DIFFERENTIATE BETWEEN SI	SMALLER THAN #200 LTS AND CLAYS

RELATIVE DENSITY OF GRANULAR SOILS

TERM"	N VALUE
VERY LOOSE	0-4
LOOSE	5-10
MEDIUM DENSE	11 – 29
DENSE	30 50
VERY DENSE THESE ARE USUALLY BASED ON AN EXAMINATION OF	OVER 50
SAMPLES, PENETRATION RESISTANCE AND SOIL DENSIT	Y DATA

RELATIVE PROPORTIONS OF COHESIONLESS SOILS

(Per ASTM D2488)

PROPORTIONAL	DEFINING RANGE BY
TERM	PERCENTAGE OF WEIGHT
TRACE	<5%
FEW	5 TO 10%
LITTLE	15 TO 25%
SOME FOR RELATIVE PERCENTAGE OF GRAV	30 TO 45% ELS, SAND AND FINES.

CONSISTENCY OF COHESIVE SOILS

-TERM	N VALUE*	STRENGTH	IDENTIFICATION PROCEDURE
		(QU, TSF)	
VERY SOFT	0-2	0 - 0.25	EASILY PENETRATED SEVERAL INCHES BY FIST.
SOFT	3-4	0.25 - 0.5	EASILY PENETRATED SEVERAL INCHES BY THUMB
MEDIUM STIFF	5-8	0.5 1.0	PENETRATED SEVERAL INCHES BY THUMB WITH
			MODERATE EFFORT.
STIFF	9 – 15	1.0 - 2.0	READILY INDENTED BY THUMB, BUT PENETRATED
			WITH GREAT EFFORT
VERY STIFF	16 – 30	2.0 - 4.0	READILY INDENTED BY THUMBNAIL
HARD	OVER 30	>4.0	INDENTED WITH DIFFICULTY BY THUMBNAIL

[&]quot;N-value correction is approximate and typically only used in absence of actual field or laboratory strength data.

RELATIVE PROPORTIONS OF COHESIONLESS SOILS

(Per ASTM D2488)

ABESENCE OF MOISTURE, DUSTY, DRY TO THE TOUCH

MOIST DAMP BUT NO VISIBLE WATER

DRY

WET VISIBLE FREE WATER, USUALLY SOIL IS BELOW WATER TABLE

SYMBOLS

DRILLING AND SAMPLING

•	RC -	ROCK CORING: SIZE NW, NX = 2-1/8" diamete
٠	RQD -	ROCK QUALITY DESIGNATION
	FT-	
٠	DC	DRIVE CASING
	C-	CASING BIZE NW. 4", HW. 6"
•	CW-	
٠	DM -	DRILLING MUD
	HAS -	HOLLOW STEM AUGER
٠	FA	
٠.	HA -	HAND AUGER
•	COA	CLEAN-OUT AUGER
	8S	2' DIAMETER SPLIT BARREL SAMPLE
		3" DIAMETER THIN-WALLED TUBE SAMPLE
٠	PT-	3° DIAMETER PISTON TUBE SAMPLE
	A5	
•	WS -	WASH SAMPLE
•	PTE -	PEAT SAMPLE
	PS -	PITCHER BAMPLE
٠	NA -	NO RECOVERY
	8-	EOUNDING:
•	PMT-	BOREHOLE PRESSUREMETER TEST
٠	VS -	
	WPT	WATER PRESSURE TEST
٠		ALL TERRAIN VEHICLE
	R-	REFUSAL CONDITION
*		
٠		
,		

LABORATORY TESTS

PP _	PENETROMETER READING, TONS/SQ. FT.
av-	UNCONFINED STRENGTH, TONS/SO, FT.
W-	MOISTURE CONTENT, %
LL-	LIQUID LIMIT, %
PL-	PLASTIC LIMIT, %
5L	EHRINKAGE LIMIT, %
1.01-	LOSS ON IGNITION, %
D-	DRY UNIT WEIGHT, LBS/CU, FT,
PH→	MEASURE OF SOIL ALKAUNITY OR ACIDITY

WATER LEVER MEASUREMENT

NW-	NO WATER ENCOUNTERED
WD-	WHILE DRILLING
BCR-	BEFORE CASING REMOVAL
ACR -	AFTER CASING REMOVAL
CM -	CAVED AND MOIST
BF -	BACKFILLED UPON COMPLETI

NOTE: WATER LEVEL MEASUREMENTS SHOWN ON THE BORING LOGS REPRESENT CONDITIONS AT THE TIME INDICATED AND MAY NOT REFLECT STATIC LEVELS, ESPECIALLY IN COHESIVE SOILS

ASTM Designation: D 2487 (Based on Unified Soil Classification System)

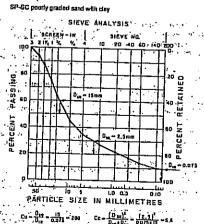
Criteria for Assigning Group Symbols and Group Names Using Labor

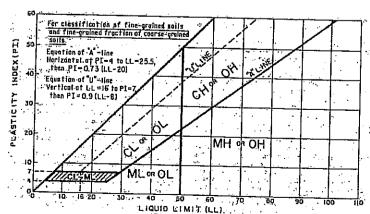
Soil Classification

Coarse-Grained Soils		Clean prayets			Graup Symbol	Group Nama A
Aora than 50% retained on No. 200 sleve	Gravels More than 50% coarse (ruction relatined on No. 4 sieve	Less Usen 5% fines ⁵	Cu ≥4 and 1 ≤ Co ≤3 [£]		GW	Well graded gravel F
			Cu < 4 and/or 1 > Cc > 1 ^E		qp	Poorly graded grayel F
		Gravels with Fines	Fines classify as ML or MH		GM	
		More that 12% fines C				SMy grave) F.C.H
			Fines classify as CL or CH		EC -	
	Sands	Clean Bands	Construction of F		SW	Cinyay Dravel F.C.H
•	More than 50% coarse fraction passes No. 4	Less than 5% fines D	Cu ≥ 6 and 1 ≤ Ca ≤ 3 ^E		200	Well praded sand ⁴
	sleve					
			Cu > 6 and/or 1 < Cc < 3 E		5P	Poorly graded sand I
		Sands with Fines	Fines classify as ML or MH		5M	
		More than 12% lines D				Silly sand G.R.I
			. Fines classify as CL or CH		SC	Clayey sand G.H.I
ne-Grained Solls PK or more passes the No. 200 sleve	Sits and Clays Liquid limit less that 50	Mergunic	PI > 7 and plots on or above "A" line	,	ČL.	Lean day K.L.u
		argenia				
			PI < 4 or plots balow "A" kno "		ML	Sil KLM
			Liquid Ernit — oven dried		OL	Organic day KLMA
			Liquid limit - not dried	<0.75		- •
	Silts and Clays	ຂາກສຽກບານ	Pi plots on or above "A" line		СН	Organic sit KLMO
	Liquid limit 50 or more				un	Fat clay K.L.M
		•	Pi piots below "A" line		МН	
		organic	Liquid limit – oven dded			Elastic silt KL4
				<0.75	OH	Organic clay K.L.M.P
			edova intili – traf dised			
hly organic soils	F	rimadly organic matter, dark in colo	f. And proprie price			Organic silt KLKO
					PT	Peat



⁸ If field sample contained cobblex or boulders, or both, add with cobbles or boulders, or both, lo group name.





C Gravels with 5 to 12% fines require dual symbols: GW-GM well-graded gravel with six

GW-GC well-graded gravel with day

GP-GM poorly graded gravel with sit

GP-GC poorly graded gravel with day

D Sands with 5 to 12% fines require dual symbols: SW-SM was graded sand with six

SW-60 well-graded sand with clay

SP-6M poorly graded sand with stit

 $^{^{\}rm F}$ If soit contains \geq 15% sand, add 'with sand' to group

 $[\]sigma$ if fines classify as CL-ML, use dual symbol GC-GM, or

H if fines are organic, add "with organic fines" to group

 $^{^{\}dagger}$ If soil contains \geq 15% gravel, and "with gravel" to group

If-Attendent limits plot in hatched area, soll is a CL-ML.

K If soil contains 15 to 20% plus No. 200, add "with send" or "with gravet," whichever is predominant.

 $^{^{}L}$ If soil contains \geq 30% plus No. 200, predominantly sand, add "sandy" to the group name.

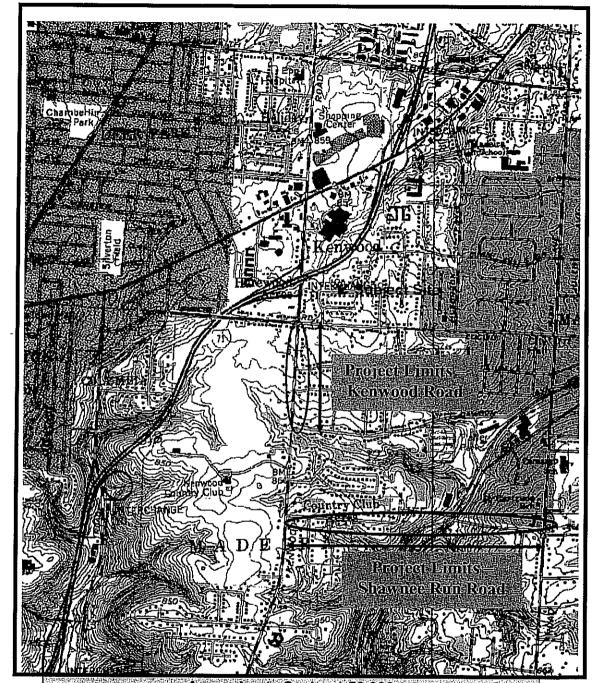
 $^{^{\}rm M}$ if soil contains \geq 30% plus No. 200, predominantly

gravel, add "gravely" to the group name. N PI≥4 and plots on or above "A" line

o Pl≤4 or plots below "A" line

P Pi plots on or above "A" line

⁹ Pt plots below "A" line

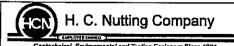


Approximate Scale: 1:50,000

Base map was copied from the U.S. Geological Survey Topographic Map of Cincinnati [East], OH Quadrangle, 1988

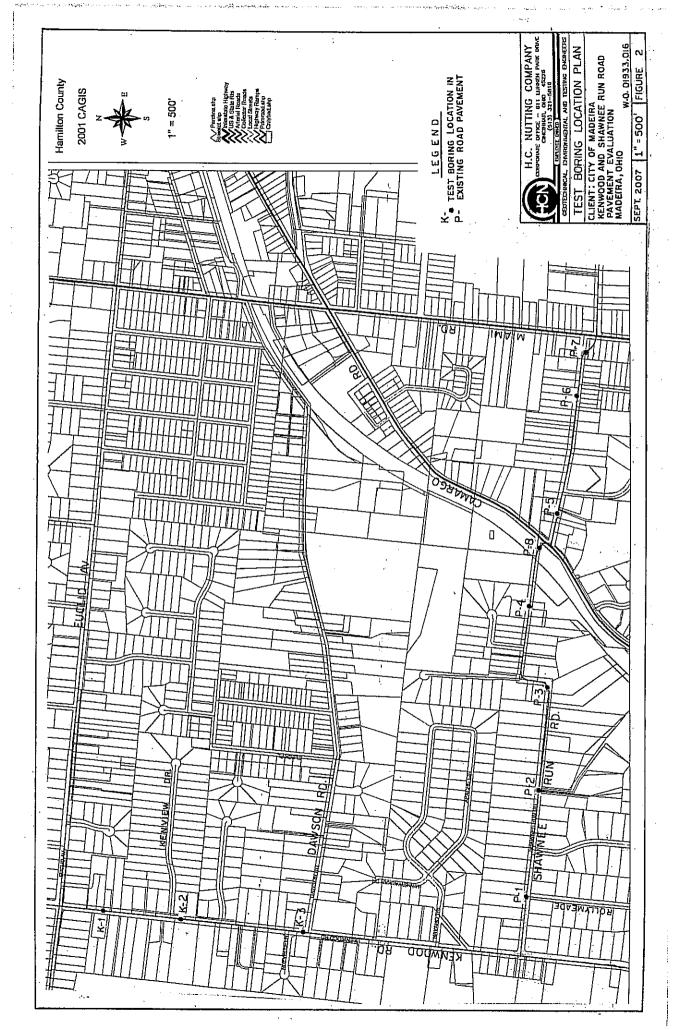


W.O. 01933.016



Site Vicinity Map
Client: City of Madeira
Project: Pavement Evaluation Study
Location: Kenwood Rd. & Shawnee
Run Rd.Madeira, OH

Figure 1





TEST BORING BORING LOGS.GPJ HC NUTTING.GDT 9/18/07

H.C. NUTTING COMPANY

CORPORATE CENTER - 811 LUNKEN PARK DRIVE CINCINNATI, OH 45226 (513) 321-5816 FAX (513) 321-0284

EMPLOYEE OWNED

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CENTRAL CHID REGION 790 MORRISON ROAD COLLMBUS, CH 43230 (514) 863-3113 FAX (614) 863-0475

INDIANA REGION BAD WALNUT STREET, STE 8 LAWRENCEBURG, DI 47025 (B12) 539-4300 FAX (B12) 539-4301

LOG OF TEST BORING

BLUEGRASS REGION 470-B CONWAY CT., STE B-B LEXINGTON, KY 40511 (859) 455-8530 FAX (859) 455-8530

Page 1 of 1

Client		_	City of Madeira			Boring No),	K-1 🕊						
Project		_	Kenwood Rd. and Shawnee Run Rd. Pavement	Evalua	tion	Date Start	_	8/31/200						
Boring (ocatic	n _	As Shown On Test Boring Location Plan			Date Com	pleted	8/31/200	7					
Elevatio						Work Orde	_	01933.0						
DEPTH				ļ	1			SAMPLE						
ft.			DESCRIPTION OF MATERIALS			DEPTH	BLOWS/6	" REC.	RQD	w	LL	PI	Qп	PPR
0.0			aterial description, moisture, stiffness/density/nardness ASPHALT PAVEMENT	NO.	TYPE	ft,	(N Value)	%	%	%	%	%	tsf	tsf
0,8 1.5	~7/	0.8	Brown medium to coarse sand, little gravel											- [
		···	(GRANULAR BASE), wet-loose					-	<u> </u>					
-		4.0	Gray clay, little sand, trace gravel (FILL), moist to very moist-stiff	1	ST	1.5-3.5	PUSHED	45		26				
		7.0		2	SS	3.5-5.0	3-2-2 (4)	80		28	Ī			2.0
7 5.5	X X		Brown and gray CLAY, trace to little sand	_3_	SS	5.0-5.5	1	100						
6.5		1.0	(GLACIAL TILL), moist-stiff to soft	ЗА	SS	5.5-6.5	1-1			25				2.0
-			BORING COMPLETED @ 6.5'		i									
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TEST BORING BORING LOGS.GPJ HC NUTTING.GDT 9/10/07

H.C. NUTTING COMPANY

CORPORATE CENTER - 811 LUNKEN PARK DRIVE CINCINNATI, OH 45226 (513) 321-5818 FAX (513) 321-0294

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APPALACHIAN REGION 812 MORRIS STREET CHARLESTON, WV 25831 (304) 344-0821 FAX (304) 342-4711 CENTRAL DHIO REGION 790 MORRISON ROAD COLLIMBUS, DH 43230 [614] 863-3113 FAX (614) 863-0475

(NDIANA REGION 349 WALNUT STREET, 8TE 8 LAWRENCEBURG, IN 47025 (812) 539-4300 FAX (812) 539-4301 BLUEGRASS REGION 470-B CONWAY CT., STE 8-8 LEXINGTON, KY 40511 (859) 455-8530 FAX (859) 455-8630

Page 1 of 1

Client			City of Madeira		-	D			V		-8-	(101/) 423-0	
		-	City of Madeira			Boring No				2 ~	<		***********	
Project		_	Kenwood Rd. and Shawnee Run Rd. Pavement	Evalua	ation	Date Star	_	8/31/200						
Boring L		-	As Shown On Test Boring Location Plan		_	Date Corr	_	8/31/200	7					l
Elevatio DEPTH	n Kef.					Work Ord		01933.01	16				,	
			DESCRIPTION OF MATERIALS	-	, 			SAMPLE			1			,]
ft.		I				DEPTH	BLOWS/6	" REC.	RQD	W	LL	PI	Qu	PPR
0.0		0.4 A	alerial description, moisture, stiffness/density/hardness ASPHALT PAVEMENT	NO.	TYPE	ft.	(N Value)	%	%	%	%	%	tsf	tsf
	(A)	0.6	(2 1/2" overlay + 2 1/2" asphalt surface with	l										
1.2		0.2	tack coat in between layers)	<u> </u>		······································						_		
	XX	2.3	CONCRETE PAVEMENT	1	ST	1.5-3,5	 PUSHED	100		29				4.0
3.5	$\langle \langle \dot{\chi} \rangle$		(with 1/4" bar reinforcing mesh)	Ĺ										7.0
⊢ <u> </u>		1.5	GRANULAR BASE	2	SS	3.5-5.0	9-10-12	67		18				4.0
5.0			Brown clay / lean clay, little silt, trace sand (FILL), moist-very stiff			0.0 0.0	(22)			10				4.0
⁻ 6.5		1.5	Brown CLAY / LEAN CLAY, little silt, trace sand	3	ss	5.0-6.5	3-3-4 (7)			21				4.0
- 0.0	DIE		and limestone fragments, moist-very stiff		\vdash		(1)		<u> </u>	_				
		1	Brown trace gray CLAY/LEAN CLAY, trace						. [
			sand, moist-very stiff BORING COMPLETED @ 6.5'											
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Rig Type		ruck						fter	-	0	_ Hr			ft.
Viethod		S/ST					W	ater used				0		ft.
nspector			·					BF = BA	CKFIL	LED	NW =	NO V	VATER	١
								(ivies	asured	HOLL C	JEOU NO	SULLS	ice)	

TEST BORING BORING LOGS.GPJ HC NUTTING.GDT 9/18/07

H.C. NUTTING COMPANY

CORPORATE CENTER - 811 LUNKEN PARK DRIVE CINCINNATI, OH 45228 (513) 321-5816 FAX (513) 321-0294

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GEOTECHNICAL, ENVIRONMENTAL AND TESTING ENGINEERS SINCE 1921 FAX 1304) 34

LOG OF TEST BORING

APPALACHIAN REGION 912 MORRIS STREET CHARLESTON, WV 25031 (304) 344-0821 FAX [304] 342-4711 CENTRAL OHIO REGION 780 MORRISON ROAD COLUMBUS, OH 41230 (614) 863-3113 FAX (614) 863-0475

INDIANA REGION 349 WALNUT STREET, STE 8 LAWRENCEBURG, IN 47025 (812) 539-4300 FAX (812) 539-4301 BLUEGRASS REGION 470-B COMWAY CT., STE 8-8 LEXINGTON, KY 40511 (859) 458-8530 FAX (859) 455-8630

Page 1 of 1

Client		_	City of Madeira				Boring No) <u>.</u>			K-	3 €	1				
Project			Kenwood Rd. and Shawnee Run Rd. Pavemen	Eva	lua	— tion	Date Start		8/3	1/200							
Boring l	_ocatio	on _	As Shown On Test Boring Location Plan				Date Com			1/200						1	
Elevatio	n Ref.					_	Work Ord	•		33.01							
DEPTH				T						IPLE							
ft.	j		DESCRIPTION OF MATERIALS				DEPTH	BLOW		REC.	RQD	W	LL	PI	Qu	PPis	
0.0			naterial description, moisture, stiffness/density/hardness	NO	o.	TYPE	ft.	(N Va		%	%	%	%	%	tsf	tsf	
0.2_/		0.2	ASPHALT PAVEMENT	/			-										
<u> </u>			CONCRETE PAVEMENT (with 1/4" bar reinforcing mesh)	<u> </u>													
- 3,5		2.7	Dark brown clay, little sand and gravel (FILL), moist-stiff	1		ST	1.5-3.5	PUSH	1ED	65		18				1.5	
_ 7_ 5.0		1.5	Brown and gray CLAY / FAT CLAY (RESIDUUM), very moist-stiff to very stiff	2	2	SS	3.5-5.0	25-16 (26		80		24				2.0	
5.7		0.7	Brown CLAY / FAT CLAY, little limestone	3	3	SS	5.0-5.7	9-50/		100		21				-	
_			\fragments (RESIDUUM), wet-very soft	$/\!$	T												
_			BORING COMPLETED @ 5.7'						ĺ								
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nspector									l B	F = BA (Me≱	CKFIL!	LED from a	NW =	: NO V	VATEF ice)	۱ ۱	
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TEST BORING BORING LOGS.GPJ HC NUTTING.GDT

H.C. NUTTING COMPANY

CORPORATE CENTER - 811 LUNKEN PARK DRIVE CINCINNATI, OH 45226 (513) 321-5816 FAX (513) 321-0294

EMPLOYEE OWNED

GEOTECHNICAL, ENVIRONMENTAL AND TESTING ENGINEERS SINCE 1921

APPALACHIAN REGION 912 MORRIS STREET CHARLESTON, WV 25031 (304) 344-0821 FAX (304) 342-4711 CENTRAL OHIO REGION 799 MORRISON ROAD COLUMBUS, OH 43230 (814) 863-3113 FAX (814) 863-0475

INDIANA REGION 349 WALNUT STREET, STE B LAWRENCEBURG, IN 47025 (B12) 539-4300 FAX (B12) 539-4301

(Measured from ground surface)

LOG OF TEST BORING

DLUEGRASS REGION 470-9 CONWAY CT., STE 9-8 LEXINGTON, KY 40511 (059) 455-6530 FAX (059) 455-8830

Clier			City of Madeira		<u></u>	Boring No	o		P-	1				
Proje		_	Kenwood Rd. and Shawnee Run Rd. Pavement	Evalu	ation	Date Star	ted s	9/4/2007	7	*****				
	ig Locat	_	As Shown On Test Boring Location Plan			Date Con		9/4/2007						
	ation Re	f.				Work Ord		01933.0						
DEP								AMPLE		•				
ft.			DESCRIPTION OF MATERIALS			DEPTH	BLOWS/6"	REC.	RQD	W	LL	Pi	Qu	PPR
0.0			naterial description, moisture, stiffness/density/hardness	NO.	TYPE	ft.	(N Value)	%	%	%	%	%	tsf	tsf
0.8		0.8	ASPHALT PAVEMENT \(1.1/4" overlay + 2.1/2" asphalt surface + 5.1/2"											
<u> </u>		10.0	(asphalt base)	/ -				-	 	<u> </u>	<u> </u>			ļ
		2.0	CRUSHED CONCRETE	/ 1	ST	1.4-3.4	PUSHED	85		24		•		2
3.4	###]	Brown and gray CLAY, trace sand and gravel, moist-stiff		<u> </u>			_						_
_			Brown CLAYEY SAND, little cobbles, trace	2	ss	3.4-4.9	6-9-9	0						
-	سببنا	3.0	gravel, wet-medium dense	-	-		(18)	+-	 	ļ				
<u> 6.4</u>	_:: <i>:</i> ::			3	SS	4.9-6.4	5-8-10 (18)	13		24				
-			BORING COMPLETED @ 6.4'				(/		 					
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	eneral l		Remarks					Wa	ter Lev	vel O	bserv	ration		
Driller		anstrati					Imn	nediate			NΝ		.c fi	t.
Rig No.		42	*Water used for pavement coring					Complet	ion _		NV		fi	
Rig Typ Method		ruck S/ST	-				Afte	er		0	Hrs		BF fi	- 1
Inspect		ו טינ						ter used				0	fi	t.
•							1	BF = BA	LKFILL	ED N	ıw = I	NO W	ATER	

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TEST BORING BORING LOGS.GPJ HC NUTTING.GDT 9/18/07

H.C. NUTTING COMPANY

CORPORATE CENTER - 811 LUNKEN PARK DRIVE CINCINNATI, OH 45226 (513) 321-5816 FAX (513) 321-0294

LOG OF TEST BORING

FAX (519) 321-0294

EMPLOYEE OWNED

GEOTECHNICAL, ENVIRONMENTAL AND TESTING ENGINEERS SINCE 1921

FAX (304) 342-4711

FAX (304) 342-4711

EIDN CENTRAL OHIO REGION ET 790 MORRISON ROAD 5031 COLUMBUS, OH 42230 (814) EE3-313 11 FAX (814) E63-0475 INDIANA REGION
349 WALNUT STREET, STE 8
LAWRENCEBURG, IN 47025
(812) 539-4300
FAX (812) 539-4301

BLUEGRASS REGION 470-B CONWAY CT., STE B-8 LEXINGTON, KY 40511 (B59) 455-8530 FAX (B59) 455-8630

CHELL		_		or iviaceira							Boring No	0.			P->	2				
Project		_	Kenw	vood Rd. a	nd Shawne	ee Run	Rd. Paveme	nt Ev	/alua	tion	Date Star	rted	8/3	30/200	7					
Boring L	.ocatio	n _	As S	hown On 1	Test Boring	Locati	on Plan				Date Con	npleted		30/200						
Elevatio	n Ref.										Work Ord	•		933,01						
DEPTH								T						VIPLE						
ft.			DE:	SCRIPTIO	N OF MAT	ERIALS	i				DEPTH	BLOW		REC.	BOD	W	LL	PI	Qu	PPR
0.0		color, m	naterial c	iescription, m	oisture, stiffn	ess/densi	ty/hardness	١,	אט	TYPE	ft.	(N Va		%	%	%		1	1	
0.5	ekilenkens	0.5	ASPI	ALT PAV	EMENT			+	.	111.2	114	(IV Va	iue)	70	70	70	%	%	tsf	tsf
<u> </u>	77	0.9	\\aspha	/erlay + 2 1 alt base)		t surfac	:e + 2 1/2"	┟											i	
	// /	2.0		KEN CON				_/	1	ST	1.4-3.4	PUSH	ΙED	100		24	26	5		0.5
<u>3.4</u>		1.5	Dark wet-s	gray silty c oft	lay, little sa	and (Fil	L), moist to	<u>.</u> }	_			3-4-	.4				2 ts	ر.		
4.9				n CLAY / L CIAL TILL)					2	SS	3.4-4.9	(8))	100		24				1
- 6.4		1.5		n LEAN CL				-/	3	SS	4.9-6.4	8-11-	·77 1	100		27				4
			\ <u>(</u> GLA(CIAL TILL)	, moist-vei	ry stiff		_/-				\ <u>\\</u>	,		<u>'</u>					
	ļ		BORI	NG COMP	LETED @	6.4'		_	- 1					i						
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	eral N						Remark	(S						Wa	ter Le	vel O	bser	vatio	ns	
Oriller	S. Wa		<u>th</u>	1/ST - Dry	Unit Weig	tht = 12	0.5 pcf						lmme	ediate	_		NV	<u> </u>	f	ft.
Rig No.		12	-				· · · · · · · · · · · · · · · · · · ·							omplet	ion		N۷	_		ft.
Rig Type		иск	_ -								•		After		_	0	_ Hr:	s	BF f	ft.
Method	SS	S/ST	-											er usec			_	0		ft.
nspector			-										В	F = BA	CKFILI	ED '	NW =	NO V	VATER	:
				•										(Mea	sured i	rom ç	iround	i surfa	ice)	

Client

H.C. NUTTING COMPANY

CORPORATE CENTER - 811 LUNKEN PARK DRIVE CINCINNATI, OH 45226 (513) 321-5818 FAX (513) 321-0294

LOG OF TEST BORING

EMPLOYEE OWNED GEOTECHNICAL, ENVIRONMENTAL AND TESTING ENGINEERS SINCE 1921

APPALACHIAN REGION 912 MORRIS STREET CHARLESTON, WV 25031 (304) 344-0821 FAX (304) 342-4711

GENTRAL OHIO REGION 780 MORRISON ROAD COLLIMBUS, OH 43230 (614) 853-3113 FAX (614) 853-0475

INDIANA REGION 349 WALNUT STREET, STE 8 LAWRENCEBURG, IN 47025 (812) 539-4300 FAX (812) 538-4301

BLUEGRASS REGION 470-B CONWAY CT., 5TE B-B LEXINGTON, KY 40511 (859) 455-8530 FAX (859) 455-8630

Client		_	City of Madeira			Boring No), ·		Р-	3			-	
Project		_	Kenwood Rd. and Shawnee Run Rd. Pavement	Evalu	ation	Date Star	ted	8/30/200)7					
Boring (_	As Shown On Test Boring Location Plan		_	Date Com	pleted	8/30/200)7					
Elevation	n Ref.					Work Ord	er No.	01933.0	16					
DEPTH								SAMPLE						
ft.		t	DESCRIPTION OF MATERIALS			DEPTH	BLOWS/	6" REC.	RQD	W	LL	Pl	Qu	PPR
0.0	_		aterial description, moisture, stiffness/density/hardness ASPHALT PAVEMENT	NO.	TYPE	ft.	(N Value	9 %	%	%	%	%	tsf	tsf
- 1.4		1.4	(2 1/2" overlay + 2 1/2" asphalt surface + 2 1/2"	ĺ				ļ						
		1.1	intermediate course + 9 1/2" asphalt base layer)	ł		:			}					
2.5	*		\BROKEN CONCRETE	<u> </u>					ļ					
		2.0	Dark brown and gray lean clay, trace sand and	1	ST	2.5-4.5	PUSHE		İ					ļ
4.5	YY	<u> </u>	gravel (FILL), moist-soft	ļ				_ _						
-			Brown and gray CLAY/FAT CLAY, moist-stiff to	2	ss	4.5-6.0	4-4-6	100		30				2
-		3.0	very stiff				(10)							
- _{7.5}				3	SS	6.0-7.5	6-8-10 (18)	100		24				3
-			BORING COMPLETED @ 7.5'				(,,,,		 	-				—
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	eral N		Remarks					Wa	ter Le	vel O	bser	vatio	15	\neg
Driller Rig No.		anstrat	*Water used for pavement coring					nmediate	_		NV			t.
tig No. tig Type		42 Tuck	-		_			t Complet	lion _		NV	***************************************	****	t.
Method		S/ST	-			·		fter <i>I</i> stor upor		0	_ Hrs		3Ff	
nspector							v	ater used BF = BA		-		NO W		t.
									sured					

H.C. NUT CORPORATE CEN CINCINNATI, FAI EMPLOYEE OWNED

H.C. NUTTING COMPANY

CORPORATE CENTER - 811 LUNKEN PARK DRIVE CINCINNATI, OH 45228 (513) 321-5818 FAX (513) 321-0294

GEOTECHNICAL, ENVIRONMENTAL AND TESTING ENGINEERS SINCE 1921

APPALACHIAN REGION
912 MORRIS STREET
CHARLESTON, WV 25031
(304) 344-0821
FAX (304) 342-4711

CENTRAL OHIO REGION TOO MORRADIM COT BESSED HO , SUBMULICO CELECESS (618) FAX (614) SE3-0475

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INDIANA REGION 348 WALNUT STREET, STE 8 LAWRENCEBURG, IN 47025 (812) 539-4300 FAX (812) 538-4301

(Measured from ground surface)

LOG OF TEST BORING

BLUEGRASS REGION 470-8 CONWAY CT., STE B-8 LEXINGTON, KY 40511 (859) 455-8530 FAX (859) 455-8630

Client City of Madeira Boring No. Project Kenwood Rd. and Shawnee Run Rd. Pavement Evaluation **Date Started** 8/30/2007 **Boring Location** As Shown On Test Boring Location Plan **Date Completed** 8/30/2007 Elevation Ref. Work Order No. 01933.016 DEPTH SAMPLE ft. **DESCRIPTION OF MATERIALS** DEPTH BLOWS/6" REC. RQD W LL ы PPR Qu color, material description, moisture, stiffness/density/hardness 0.0 NO. TYPE fŁ (N Value) % % % % tsf tsf ASPHALT 8.0 0.8 0.6 **GRANULAR BASE** Brown and gray clay / fat clay, trace limestone fragments (FILL), moist-stiff 1 ST 1.5-3,5 **PUSHED** 25 19 3.6 4-9-10 2 SS 3.5-5.0 20 30 5.0 2.0 (19) Brown trace gray CLAY, some silt, little 1.5 8-11-31 limestone fragments (RESIDUUM), moist-very 3 SS 5.0-6.5 87 18 3.5 6.5 (42)BORING COMPLETED @ 6.5' **General Notes** Remarks Water Level Observations Driller B. Wallace 1/ST - Dry Unit Weight = 103.8 pcf Immediate NW ft. Rig No. B-57 At Completion NW ft. Rig Type Truck After 0 ft. Hrs. Method SS/ST Water used in drilling ft. Inspector BF = BACKFILLED NW = NO WATER

EMPLOYEE OWNED

TEST BORING BORING LOGS,GPJ

H.C. NUTTING COMPANY

CORPORATE CENTER - 611 LUNKEN PARK DRIVE CINCINNATI, OH 45226 (513) 321-5816 FAX (513) 321-0294

GEOTECHNICAL, ENVIRONMENTAL AND TESTING ENGINEERS SINCE 1921

AFPALACHIAN REGION 012 MORRIB STREET CHARLESTON, WV 25031 (304) 344-0821 FAX (304) 342-4711

CENTRAL OHIO REGION TO ROBRISON POR TO EVER (418) CELE-CER (418) FAX (614) SE3-0475

INDIANA HEGION 349 WALNUT STREET, STE 8 LAWRENCEBURG, IN 47025 (812) 539-4300 FAX (812) 539-4301

LOG OF TEST BORING

BLUEGRASS REGION 470-9 COMWAY CT., STE 9-8 LEXINGTON, KY 40511 (859) 455-8530 FAX (859) 455-8630

Client		-	City of Madelra			Boring No	o		P-	5				
Project		_	Kenwood Rd. and Shawnee Run Rd. Pavemen	t Evalu	ation	Date Star	ted s	9/4/2007	,					
Boring		_	As Shown On Test Boring Location Plan			Date Con	pleted 9	7/4/2007	,					
Elevation					_	Work Ord		1933.0						
DEPTH								AMPLE						
ft.			DESCRIPTION OF MATERIALS			DEPTH	BLOWS/6"		RQD	W	LL	PI	Qu	PPR
0.0]	color, n	naterial description, moisture, stiffness/density/hardness	NO.	TYPE		(N Value)	%	%	%	%	%	tsf	l
0.9		0.9	ASPHALT PAVEMENT				(1, 10,00)	- "	-/ <u>-</u> -	1-78	"	70	เธเ	tsf
1.3	ai w	0.4		┧						<u> </u>				
- - 3.3		2.0	Brown trace gray LEAN CLAY, moist to very moist-medium stiff to very soft	1	ST	1.3-3,3	PUSHED	100		25	32	16		0.25
			Brown CLAY / FAT CLAY, trace sand, moist-very stiff	2	ss	3.3-4.8	4-7-10 (17)	100	 	26				3.5
- - 6.3		3.0		3	SS	4.8-6.3	8-12-14 (26)	33		26				2.5
9.5	1131111		BORING COMPLETED @ 6.3'	+			(20)	_	 		-			
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Rig No.		12						Comple			NV NV			t.
Rig Type		uck		****			Afte		-	0	Hr			1.
Method		/ST						iter used	in dri		_ ' *''	<u>, </u>		t.
Inspector								BF = BA	CKFILL	LED	NW =	NO V	VATER	
								(Mea	asured t	from ç	round	surfa	ce)	

(tCI)

TEST BORING BORING LOGS.GPJ HC NUTTING.GDT 9/18/07

H.C. NUTTING COMPANY

CORPORATE CENTER - 611 LUNKEN PARK DRIVE CINCINNATI, OH 45228 (513) 321-5816 FAX (513) 321-0294

EMPLOYEE OWNED

GEOTECHNICAL, ENVIRONMENTAL AND TESTING ENGINEERS SINCE 1921

LOG OF TEST BORING

AFPALACHIAN REGION 912 MORRIS STREET CHARLESTON, WV 25031 (304) 344-0821 FAX (304) 342-4711 CENTRAL CHIO REGION 790 MORRISON ROAD COLUMBUS, OH 43230 (514) 863-3113 FAX (614) 863-0475

INDIANA REGION 349 WALNUT STREET, 81E 8 LAWRENGEBURG, IN 47025 (812) 539-4300 FAX (812) 539-4301 BLUEGRASS REGION 470-8 CONWAY CT., STE 8-8 LEXINGTON, KY 40511 (859) 455-8530 FAX (859) 455-8330

Client	City	of Madeira			Boring No).	-	P-(6				
Project	Ken	wood Rd. and Shawnee Run Rd. Pavement	Evalua	ation	Date Star	_	9/4/2007						
Boring Location	л <u>As 5</u>	Shown On Test Boring Location Plan		_	Date Com	_	9/4/2007						
Elevation Ref.	<u> </u>				Work Ord	_	01933.01						
DEPTH	-	ECODIDION OF MATTER A					AMPLE			,			
ft.		ESCRIPTION OF MATERIALS			DEPTH	BLOWS/6	" REC.	RQD	W	LL	PI	Q	PPR
0.0		description, moisture, stiffness/density/hardness	NO.	TYPE	ft.	(N Value)	<u>%</u>	%	%	%	%	tsf	tsf
- 1.4 3 3	07\(11	/4" overlav + 3 3/4" asphalt surface + 3 1/2" .											
- 2.3		half base)	1	ST	1.4-1.8	PUSHEL			15				
- 3.3		NCRETE PAVEMENT wn gravel and cobbles, trace sand	2 2A	SS	1.8-2.3 2.3-3.3	12 4-3	100 50		15) 30				1.0
	15 ∬(GR.	ANULAR BASE), wet-loose to medium	3	SS		4-6-8							1
4.8	<u> uens</u>		3	33	3.3-4.8	(14)	27		25				
- 6.3	'.J grav	vn and gray clay/fat clay, trace sand and rel (FILL), moist-medium stiff	4	SS	4.8-6.3	35-15-44 (59)	87		20				0.5
-	Brov very	vn and gray clayey sand and gravel (FILL), molst-medium dense											
-	\fragr \FILL	vn trace gray clay, trace to little limestone ments and shale fragments (POSSIBLE), very moist-soft			:								
- -	BOR	RING COMPLETED @ 6.3'											ĺ
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Method SS	/ST						ier ater usec	d in dri		— _{пв}	s		t.
Inspector							BF = BA	CKFILI	ED		NO V	VATER	
		1					(Mea	sured	from g	round	i surfa	ce)	

EMPLOYEE OWNED

H.C. NUTTING COMPANY

CORPORATE CENTER - 811 LUNKEN PARK DRIVE CINCINNATI, OH 45226 (513) 321-5818 FAX (513) 321-0294

GEOTECHNICAL, ENVIRONMENTAL AND TESTING ENGINEERS SINCE 1921

APPALACHIAN REGION 012 MORRID STREET CHARLESTON, WV 25031 (304) 344-0821 FAX (304) 342-4711

CENTRAL CHIO REGION 780 MORRISON ROAD COLUMBUS, OH 43230 (814) 883-3112 FAX (614) 863-0475

INDIANA REGION 349 WALNUT STREET, SIE B LAWRENCEBURG, IN 47025 (812) 539-4300 FAX (812) 539-4301

LOG OF TEST BORING

BLUEGRASS REGION 470-8 CONWAY CT., 5TE B-8 LEXINGTON, KY 40511 (859) 455-0530 FAX (850) 455-0630

Cilent		-	City of Madelia			Boring No),		<u>P-</u>					i
Project		_	Kenwood Rd. and Shawnee Run Rd. Pavement	Evalua	ation	Date Start	ted	9/4/200	7					
Boring L		_	As Shown On Test Boring Location Plan		_	Date Com	pleted	9/4/200						
Elevatio						Work Ord	er No.	01933.0						
DEPTH	1							SAMPLE	_					
ft.			DESCRIPTION OF MATERIALS			DEPTH	BLOWS		RQD	W	LL	PI	Qu	PPR
0.0			naterial description, moisture, stiffness/density/hardness	NO.	TYPE	ft.	(N Valu		%	%	%	%	tsf	tsf
0.6		0.6	ASPHALT PAVEMENT				,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	' '				,,,	101	LOI
_ 2.1		1.5	\(3 1/2" overlay + 3 1/2" asphalt surface) Brown fine to medium sand, little gravel and						1					
<u>ــ ۲۰۱</u>	'		cobbles (GRANULAR BASE)						-	<u> </u>	ļ			
⊢ .			Brown LEAN CLAY, some silt, little sand	1	ST	2.1-4.1	PUSH	ED 30		24			İ	
-		3.5	(GLACIAL TILL), moist-very stiff				1 33111			27			ļ	
				2	ss	4.1-5.6	6-8-1	2 100	Ï	17				
5.6			Brown CLAY, little sand, trace gravel (GLACIAL			.,, 0.0			ļ	<u> '' </u>				4.0
_ _ 7.1		1.5	TILL), moist-very stiff	3	ss	5.6-7.1		4 87		26		ĺ		4.0
- ''	التلبيد	_	BORING COMPLETED @ 7.1'				(23)		-					
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nspector								BF = B/	CKFILI	LED I	NW =	NO W	VATER	
								(Me	asured	from g	round	surfa	ce)	I

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TEST BORING BORING LOGS.GPJ HC NUTTING.CDT 9/18/07

H.C. NUTTING COMPANY

CORPORATE CENTER - 811 LUNKEN PARK DRIVE CINCINNATI, OH 45226 (513) 321-5816 FAX (513) 321-0284

EMPLOYEE OWNED

GEOTECHNICAL, ENVIRONMENTAL AND TESTING ENGINEERS SINCE 1921

LOG OF TEST BORING

APPALACHIAN REGION B12 MORRIS STREET CHARLESTON, WV 25031 (304) 344-0821 FAX (304) 342-4711 CENTRAL OHIO REGION 790 MORRISON ROAD COLUMBUS, OH 43230 (514) 863-3113 FAX (614) 863-0475

INDIANA REGION 349 WALKUT STREET, STE 8 LAWRENCEBURG, IN 47025 (812) 539-4300 FAX (812) 539-4301 BLUEGRASS REGION 470-B CONWAY CT., STE B-1 LEXINGTON, KY 40511 (859) 455-8530 FAX (859) 455-8630

Client			City of Madeira		***	Boring No).		P-	R			109) 400-6	
Project		-	Kenwood Rd. and Shawnee Run Rd. Pavement	Evalua	 ation	Date Star		4/2007		<u> </u>				
Boring	Location	תכ	As Shown On Test Boring Location Plan			Date Corr		4/2007						
Elevation	on Ref				 .	Work Ord		1933.0						
DEPTH				T		TTOIR OIL		MPLE	10					
ft.			DESCRIPTION OF MATERIALS			DEPTH	BLOWS/6"		RQD	W	LL	PI	0	DDD
0.0]	color, n	naterial description, moisture, stiffness/density/hardness	No.	TYPE	1	(N Value)	%	l	%			Qu	PPR
0.6		0.6	ASPHALT PAVEMENT	1	<u> </u>	- /.	(IN VAIUE)	70	%	70	-%	%	tsf	tsf
1.4	5	0.8	GRANULAR BASE]					[İ				
- - 3.5		2.1	Dark gray clay with organics, wood fragments and root matter (FILL), moist-soft	1	ST	1.5-3.5	PUSHED	60		34			-	
 5.0		1.5	Brown CLAY/FAT CLAY, trace sand (RESIDUUM), moist-very stiff	2	ss	3.5-5.0	5-5-6 (11)	67		22				4.0
5.8	ш	0.8	Brown and gray CLAY/FAT CLAY, little	3	SS	5,0-5,8	17-50/0.3	100		21				4.0
Γ		,	limestone fragments (RESIDUUM), moist-very stiff	1										
T			BORING COMPLETED @ 5.8'	•										
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Ger	neral N	lotes	Remarks				···				L			
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Rig No.		-57	J. J. J. J. J. J. J. J. J. J. J. J					ediate omplet	ion -		NV NV			t. t.
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Method		S/ST	_					er usec	i in dri		- '"	" _	<u></u> - f	i i
Inspector	·		-					BF = BA	CKFILI	.ED I	NW =	NO V	VATER	
								(Mea	sured l	rom g	round	surfa	ce)	

H.C. Nutting Company 611 Lunken Park Dr. Cincinnati, Ohio 45226 City of Madeira, Ohio Kenwood & Shawnee Run Road Madeira, Ohio HCN W.O. #01933.016

TABLE I: CLASSIFICATION TEST DATA

				At	terberg Li	mits		
Boring No.	Sample No.	Depth (ft.)	Moisture Content %	Liquid Limit %	Plastic Limit %	Plasticity Index	Maximum Dry Density (pcf)	Optimum Moisture Content (%)
(K-1	2	3.5-5	27.7					
	3	5-6.5	25.1					
(K-2	2	3.5-5	18.4					
	3	5-6.5	21.1					
(K-3)	2	3.5-5	23.5					
	3	5-6.5	21.2					
			-					
P-1	3	4.9-6.4	23.7					
P-2	ST-1	1.4-3.4	24.1	26	21	5		
	2 ·	3.4-4.9	24.2			,		
	3	4.9-6.4	27.3					
P-3		450	20.4					
P-3	<u>2</u> 3	4.5-6	30.4					
<u></u>	3	6-7.5	23.6					
P-4	2	3.5-5	29.9					
	3	5-6.5	18.0	·				
			10.0					
P-5	ST-1	1.3-3.3	24.8	32	16	16		
	2	3.3-4.8	26.2					
	3	4.8-6.3	25.9					
P-6	2	1.8-2.3	14.5					
	2A	1.8-2.3	29.6					
	3	3.3-4.8	24.7				·	
	4	4.8-6.3	25.9					
							-	

H.C. Nutting Company 611 Lunken Park Dr. Cincinnati, Ohio 45226

City of Madeira, Ohio Kenwood & Shawnee Run Road Madeira, Ohio HCN W.O. #01933.016

TABLE I: CLASSIFICATION TEST DATA

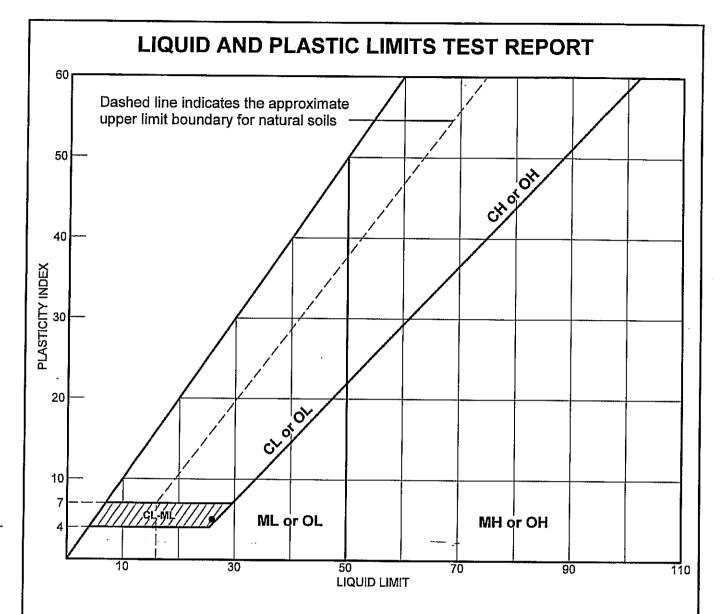
			At	terberg Li	mits		
Sample No.	Depth (ft.)	Moisture Content %	Liquid Limit %	Plastic Limit %	Plasticity Index	Maximum Dry Density (pcf)	Optimum Moisture Content (%)
2	4.1-5.6	16.8					
3	5.6-7.1	26.3					
2	3.5-5	21.8					
3	5-6.5	20.5					
BS-2 (Bag)	1.5-5	<u>-</u> _	33	17	16	108.6	16.7
BS-3 (Bag)	1.5-5		39	18	21	107.2	18.6
BS-1 (Bag)	1.5-5		37	18	19	109.5	16.9
	2 3 2 3 BS-2 (Bag) BS-3 (Bag)	No. (ft.) 2 4.1-5.6 3 5.6-7.1 2 3.5-5 3 5-6.5 BS-2 (Bag) BS-3 (Bag) BS-1 1.5-5	No. (ft.) Content % 2 4.1-5.6 16.8 3 5.6-7.1 26.3 2 3.5-5 21.8 3 5-6.5 20.5 BS-2 (Bag) 1.5-5 BS-3 (Bag) 1.5-5	Sample No. Depth (ft.) Moisture Content % Liquid Limit % 2 4.1-5.6 16.8 3 3 5.6-7.1 26.3 2 3.5-5 21.8 3 5-6.5 20.5 BS-2 (Bag) 1.5-5 39 BS-3 (Bag) 1.5-5 37	Sample No. Depth (ft.) Moisture Content % Liquid Limit % Plastic Limit % 2 4.1-5.6 16.8 3 5.6-7.1 26.3 3 2 3.5-5 21.8 3 3 5-6.5 20.5 3 17 BS-2 (Bag) 1.5-5 39 18 BS-3 (Bag) 1.5-5 37 18	No. (ft.) Content % Limit % Limit % 2 4.1-5.6 16.8 3 5.6-7.1 26.3 2 3.5-5 21.8 3 5-6.5 20.5 BS-2 (Bag) 1.5-5 33 17 16 BS-3 (Bag) 1.5-5 39 18 21	Sample No. Depth (ft.) Moisture Content % Liquid Limit % Plastic Limit % Plasticity Index Maximum Dry Density (pcf) 2 4.1-5.6 16.8 3 5.6-7.1 26.3 3 5.6-7.1 26.3 3 5.6-7.1 26.3 3 1.5-5 3 3 17 16 108.6 108.6 108.6 107.2 107.2 107.2 109.5

H.C. Nutting Company 611 Lunken Park Dr. Cincinnati, Ohio 45226

City of Madeira, Ohio Kenwood & Shawnee Run Road Pavement Evaluation Madeira, Ohio HCN W.O. #01933.016

TABLE II: TABULATION OF UNDISTURBED DATA (UNIT WEIGHT)

Boring	Sample No.	Depth (ft.)	Material Description	Dry Density (pcf)	Water Content (%)
(K-1)	ST-1	1.5-3.5	Lean clay	97.7	25.8
(K-2)	ST-1	1.5-3.5	Clay	95.7	28.5
(K-3)	ST-1	1.5-3.5	Lean clay	104.6	18.0
P-1	ST-1	1.4-3.4	Lean clay	99.8	23.9
P-2	ST-1	1.4-3.4	Lean clay	120.5	24.1
P-3	ST-1	2.5-4.5	No Recovery		
P-4	ST-1	1.5-3.5	Clay	- 103.8	18.9
P-5	ST-1	1.3-3.3	Lean clay	101.7	24.8
P-6	ST-1	1.4-1.8	No Recovery		
P-7	ST-1	2.1-4.1	Lean clay	101.3	23.5
P-8	ST-1	1.5-3.5	Clay	69.1	34.1



	SOIL DATA								
SYMBOL	SOURCE	SAMPLE NO.	DEPTH (ft.)	NATURAL WATER CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	USCS	
•	P-2	ST-1	1.4-3.4		21	26	5		

LIQUID AND PLASTIC LIMITS TEST REPORT

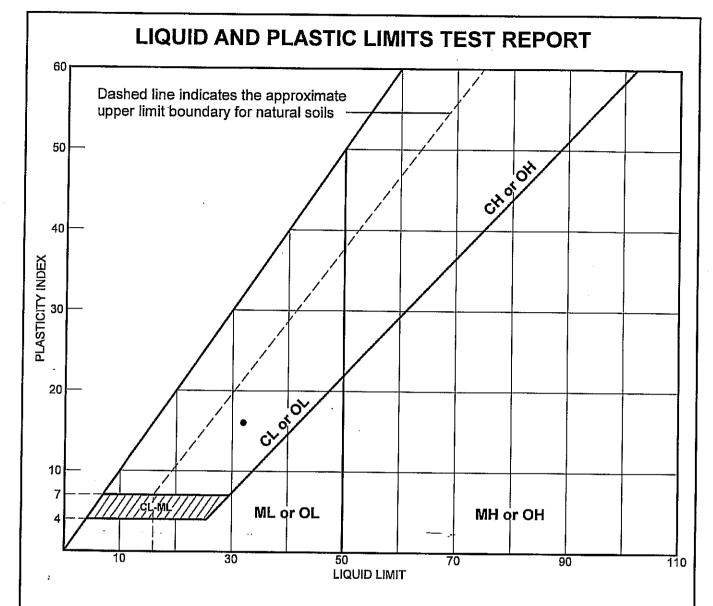
H. C. NUTTING COMPANY

Client: CITY OF MADEIRA, OHIO

Project: KENWOOD AND SHAWNEE RUN RD. PAVEMENT EVAL.

Project No.: 01933.016

Figure 9803



				SOIL DATA				
SYMBOL	SOURCE	SAMPLE NO.	DEPTH (ft.)	NATURAL WATER CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	uscs
•	P-5	ST-1	1.3-3.3'		16	32	16	

LIQUID AND PLASTIC LIMITS TEST REPORT

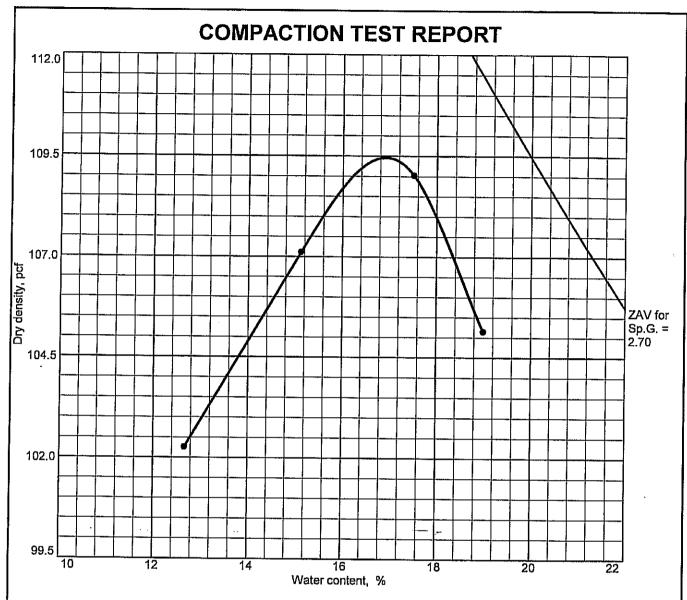
H. C. NUTTING COMPANY

Client: CITY OF MADEIRA, OHIO

Project: KENWOOD AND SHAWNEE RUN RD. PAVEMENT EVAL.

Project No.: 01933.016

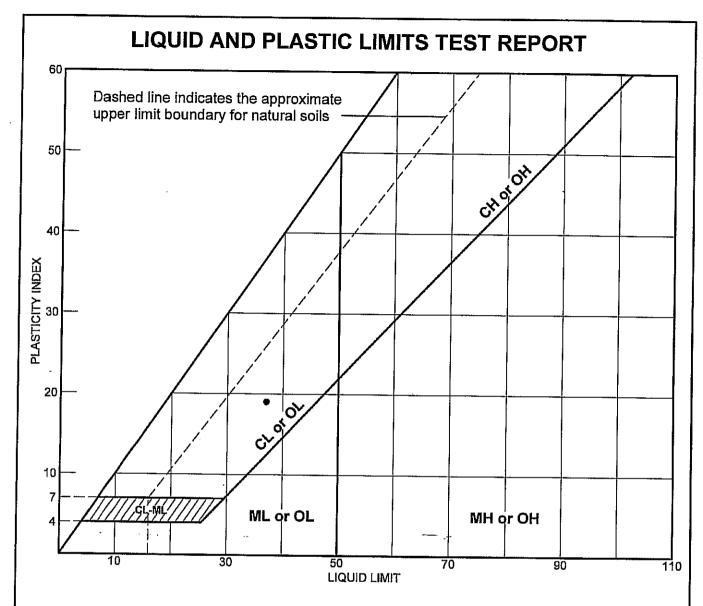
Figure 9809



Test specification: ASTM D 698-00 Procedure B Standard

Elev/	Classi	Nat.	Sp.G.			%>	% <	
Depth	USCS	AASHTO.	Moist.	Sp.G.		PI	3/8 in.	No.200
1.5-5'		1			37	19		

TEST RESULTS	MATERIAL DESCRIPTION
Maximum dry density = 109.5 pcf	BROWN LEAN CLAY
Optimum moisture = 16.9 %	
Project No. 01933.016 Client: CITY OF MADEIRA, OHIO	Remarks:
Project: KENWOOD AND SHAWNEE RUN RD. PAVEMENT EVAL.	DATE TYPED 9-12-07 TESTED BY EJ
• Source: K1,K2,K3 Sample No.: BS-1 Elev./Depth: 1	.5-5'
COMPACTION TEST REPORT	
H. C. NUTTING COMPAN	Y Figure 9772



	SOIL DATA								
SYMBOL	SOURCE	SAMPLE NO.	DEPTH (ft.)	NATURAL WATER CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	USCS	
•	K1,K2,K3	BS-1	1.5-5'		18	37	19		

LIQUID AND PLASTIC LIMITS TEST REPORT

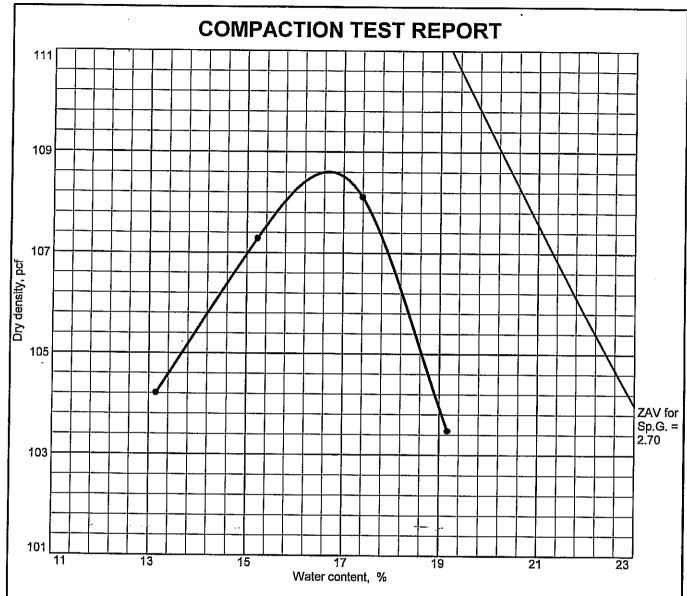
H. C. NUTTING COMPANY

Client: CITY OF MADEIRA, OHIO

Project: KENWOOD AND SHAWNEE RUN RD. PAVEMENT EVAL.

Project No.: 01933.016

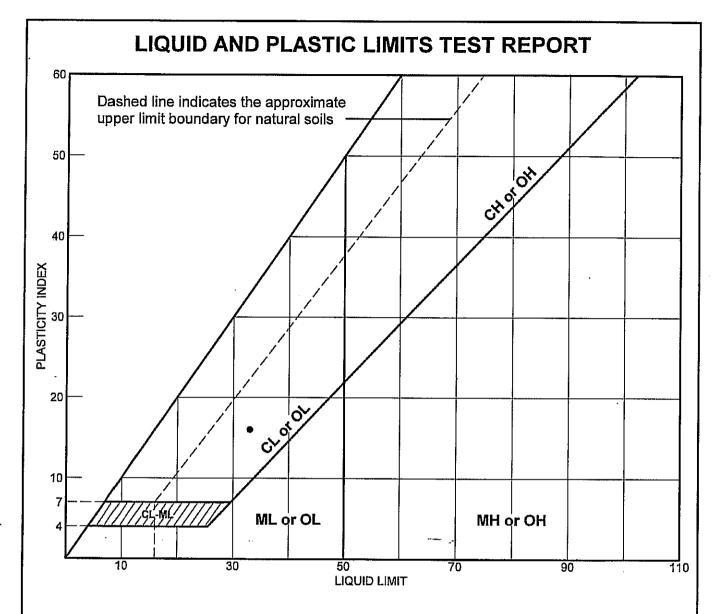
Figure 9772



Test specification: ASTM D 698-00 Procedure B Standard

Elev/	ev/ Classification		Nat.		LL		% >	% <
Depth	USCS	AASHTO	Moist.	Sp.G.	LL 	PI	3/8 in.	No.200
1.5-5'					33	16		

TEST RESULTS	MATERIAL DESCRIPTION
Maximum dry density = 108.6 pcf	BROWN LEAN CLAY
Optimum moisture = 16.7 %	
Project No. 01933.016 Client: CITY OF MADEIRA, OHIO	Remarks:
Project: KENWOOD AND SHAWNEE RUN RD. PAVEMENT EVAL.	DATE TYPED 9-11-07 TESTED BY EJ
 Source: P1,P2,P3 Sample No.: BS-2 Elev./Depth: 	1.5-5'
COMPACTION TEST REPORT	· ·
H. C. NUTTING COMPAN	Figure 9770



				SOIL DATA				
SYMBOL	SOURCE	SAMPLE NO.	DEPTH (ft.)	NATURAL WATER CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	USCS
•	P1,P2,P3	BS-2	1.5-5'		17	33	16	

LIQUID AND PLASTIC LIMITS TEST REPORT

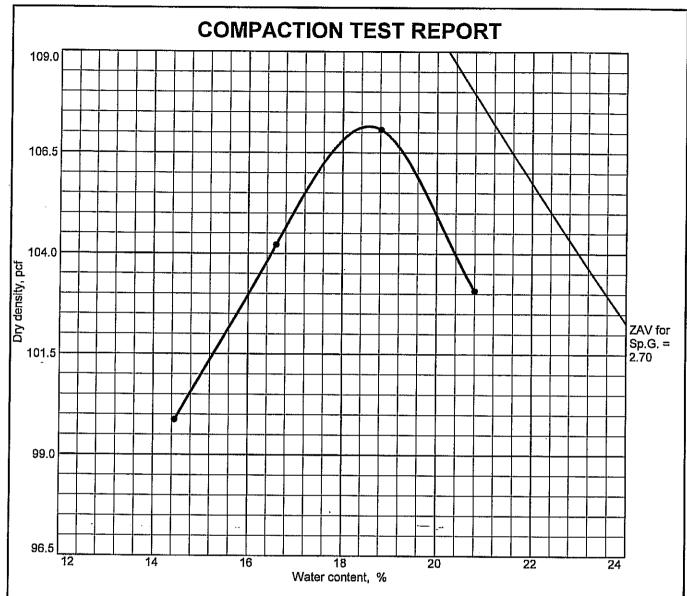
Client: CITY OF MADEIRA, OHIO

H. C. NUTTING COMPANY

Project: KENWOOD AND SHAWNEE RUN RD. PAVEMENT EVAL.

Project No.: 01933.016

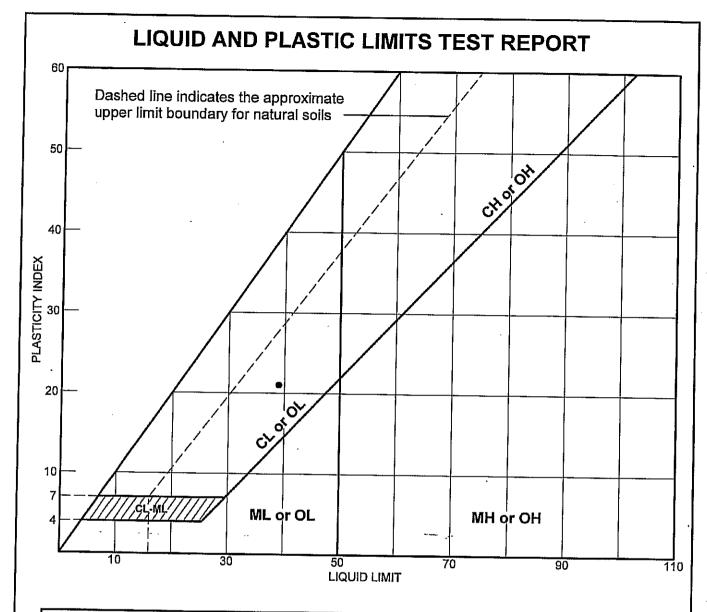
Figure 9770



Test specification: ASTM D 698-00 Procedure B Standard

Elev/	Classification			Sp.G.	LL	ы	% >	% <
Depth	USCS	AASHTO	Moist.	Sp.G.	LL.	PI	3/8 in.	No.200
1.5-5'					39	21		•

	TEST RESULTS		MATERIAL DESCRIPT	TION	
Maximum dry density = 107.2 pcf			BROWN LEAN CLAY		
Optimum moisture = 1	8.6 %				
Project No. 01933.016	Client: CITY OF MADEIRA, C	Remarks:			
Project: KENWOOD AN	ID SHAWNEE RUN RD. PAVEME	NT EVAL.	DATE TYPED 9-12-07 TESTED BY EJ		
• Source: P5,P6,P7	Sample No.: BS-3 EI	ev./Depth: 1.5-5			
	COMPACTION TEST REPORT		· ·		
H. C. N	JUTTING COM	IPANY	Figure	9771	



				SOIL DATA	\			······
SYMBOL	SOURCE	SAMPLE NO.	DEPTH (ft.)	NATURAL WATER CONTENT (%)	PLASTIC LIMIT (%)	LIQUID LIMIT (%)	PLASTICITY INDEX (%)	USCS
	P5,P6,P7	BS-3	1.5-5'		18	39	21	-

LIQUID AND PLASTIC LIMITS TEST REPORT

Client: CITY OF MADEIRA, OHIO

H. C. NUTTING COMPANY

Project: KENWOOD AND SHAWNEE RUN RD. PAVEMENT EVAL.

Project No.: 01933.016

Figure 9771

GEOTECHNICAL ENVIRONMENTAL AND TESTING ENGINEERS

CORPORATE CENTER 611 LUNKEN PARK DRIVE CINCINNATI, OHIO 45226 (513) 321-5816 FAX (513) 321-0294

SAMPLE DISPOSITION

Unless other arrangements are made with H. C. Nutting Company (HCN), all soil and rock core samples collected during the course of this work will be disposed of 30 days after our report or lab test result submittal.

If the client wishes to avoid sample disposal in 30 days, other arrangements can be made, including any of the following:

- The samples may be picked up by the client's representative from HCN's office, as prescheduled with HCN. The pick up date must precede the 30-day limit described above.
- 2. The samples can be shipped to the client by HCN. All costs associated with shipping shall be borne by the client.
- 3. The samples can be stored by HCN at a cost borne by the client. This cost will be based on the type of samples stored (boxes of soil sample jars, rock core boxes, etc.) and the duration of storage. Specific needs for sample storage beyond 30 days shall be detailed in the contract at agreed upon rates.

Requested Alternate Action:

Sample (arrange	to be picked up by Client nents will be coordinated with Laboratory Manager	-)
Sample:	to be shipped to:borne by client)	
Samples	to be stored by HCN at negotiated rates	
	cknowledgment:	
	ompany:	
!	ame:	
:	ignature:	
	ate:	

Please return this form to: H.C. Nutting Co. 611 Lunken Park Dr. Cincinnati, OH 45226 Attn: Laboratory Manager Phone: (513) 321-5816, Fax: (513) 321-0294